# SUCCESSFUL AMS <sup>14</sup>C DATING OF NON-HYDRAULIC LIME MORTARS FROM THE MEDIEVAL CHURCHES OF THE ÅLAND ISLANDS, FINLAND

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**ABSTRACT**. Fifteen years of research on accelerator mass spectrometry (AMS) radiocarbon dating of non-hydraulic mortar has now led to the establishment of a chronology for the medieval stone churches of the Åland Islands (Finland), where no contemporary written records could shed light on the first building phases. In contrast to other material for dating, well-preserved mortar is abundantly available from every building stage.

We have gathered experience from AMS dating of 150 Åland mortar samples. Approximately half of them have age control from dendrochronology or from <sup>14</sup>C analysis of wooden fragments in direct contact with the mortar. Of the samples with age control, 95% of the results agree with the age of the wood. The age control from dendrochronology, petrologic microscopy, chemical testing of the mortars, and mathematical modeling of their behavior during dissolution in acid have helped us to define criteria of reliability to interpret the <sup>14</sup>C results when mortar dating is the only possibility to constrain the buildings in time. With these criteria, 80% of all samples reached conclusive results, and we have thus far been able to establish the chronology of 12 out of the 14 churches and chapels, while 2 still require complementary analyses.

### INTRODUCTION

For decades, the chronology of the medieval churches of the Åland Islands, Finland, has been the subject of a heated debate. With the aim to solve this problem and create an objective chronology for the 12 medieval stone churches and 2 chapels, the project "The Churches of the Åland Islands" was initiated in 1990. Different scientific methods were applied, initially with focusing on dendrochronology and conventional radiocarbon dating of mortar. In 1994, the introduction of AMS <sup>14</sup>C analysis presented a new opening, resulting in the interdisciplinary *International Mortar Dating Project*. Our methodological and theoretical development efforts have been the subject of a dissertation (Lindroos 2005) and have also been published in different scientific and archaeological journals and monographs as well as proceedings of international conferences (e.g. Ringbom and Remmer 1995, 2000, 2005; Heinemeier et al. 1997; Hale et al. 2003; Ringbom et al. 2006, 2009; Lindroos et al. 2007). We have also extended the application of mortar dating to mortars of Roman ruins in Portugal (Langley et al. 2010) and Rome (Hodgins et al. 2010; Lindroos et al. 2010; Ringbom et al. 2010), where the hydraulic nature (Borrelli 1999) of the pozzolana mortar makes the interpretation more complex than in the case of the Åland churches. In the present paper, we focus on the results and lessons of the non-hydraulic mortars of Åland.

The incentive to develop and use the costly <sup>14</sup>C mortar dating technique to resolve the chronology of the Åland churches has been the general lack of alternatives:

- There are no preserved historical sources to shed light on the chronology of the Åland churches;
- Coins and archaeological artifacts do not date mortared structures;
- Only few datable materials are available;
- Dendrochronology was performed on all the churches in 1991–1992. However, due to the early
  timber constructions having been consumed by fires or rot, the result was disappointing since it
  did not date the original structures, only secondary building stages (towers) and later repairs;
- There are essentially no brick constructions and thus thermoluminescence dating has not been an option.

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In contrast to all other datable materials, there is always plenty of original mortar from every stage of the building construction, which naturally makes successful mortar dating techniques very rewarding, offering a potential key to classical and medieval archaeology. Throughout, we have supplemented this with dating of alternative materials, such as inclusions in the mortar of charcoal for control purposes, but we have generally seen confirmation of the findings of others (e.g. Tubbs and Kinder 1990) that charcoal inclusions often are far older than the mortar. By contrast, carefully selected samples of wood fragments from the surface of scaffolding or from timber embedded in the mortar during construction have turned out to be useful. Here, we present the full series of dating measurements from the Åland Islands, the inferred dates of each building unit compared to independent, science-based chronological evidence, mainly dendrochronology and <sup>14</sup>C analysis of wood, where available. Finally, we give an overview of the resulting chronology of the 12 churches and chapels dealt with so far out of the 14 existing in the Åland Islands.

### **BACKGROUND**

The principle of the method of dating lime mortars using standard <sup>14</sup>C carbonate procedures has been known since the 1960s (Labeyrie and Delibrias 1964; Stuiver and Smith 1965; see Figure 1).

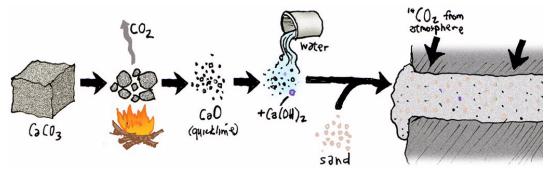


Figure 1 Mortar absorbs carbon dioxide from the atmosphere when it hardens, which makes it potentially suitable for <sup>14</sup>C dating (from Hale et al. 2003, with modifications).

Atmospheric carbon dioxide is fixed in the carbonate formed during the hardening of lime mortar at the time of construction, which in principle makes it ideally suited for <sup>14</sup>C dating. To produce building lime, limestone is heated to at least 900 °C to liberate carbon dioxide and produce quicklime (calcium oxide, CaO). The quicklime is then slaked with water to form calcium hydroxide (Ca(OH)<sub>2</sub>) or building lime, which is mixed with aggregates or filler (sand) and water to form mortar. Calcium hydroxide in mortar reacts with atmospheric carbon dioxide forming calcium carbonate (CaCO<sub>3</sub>), as the binder in the hardened mortar. The <sup>14</sup>C content of a mortar sample can thus in principle give a measure of the time elapsed since the time of hardening.

There are, however, well-known risks associated with the method as it is sensitive to contamination effects that have been poorly understood and it has therefore been used with precaution and with varying success in archaeometry (e.g. Baxter and Walton 1970; Folk and Valastro 1976; Van Strydonck et al. 1983; Willaime et al. 1983). The mortar may contain old limestone, either as remains from incomplete conversion into calcium oxide in the burning process or from sedimentary carbonate in the aggregate, yielding apparent ages that are too old due to this form of contamination. Conversely, delayed hardening in thick walls or later recrystallization of the carbonate incorporating younger carbon dioxide can lead to dates that are too young. Some systematic studies of mortar

hardening and dissolution versus chemical activity of stable isotopes have been published (Pachiaudi et al. 1986; Van Strydonck et al. 1986, 1989; Ambers 1987; Van Strydonck and Dupas 1991; Sonninen and Jungner 2001), but the link to carbonate mineralogy and stable isotope geochemistry has been dealt with in more detail (Létolle et al. 1990; Lindroos 2005; Lindroos et al. 2007).

Concerning sampling strategy, it is important to avoid secondary repairs. In the Åland churches, most sampling has taken place under roofs in sheltered places. The sample is taken carefully with a chisel from the surface, where the mortar has hardened quickly. First, the outermost layer is gently cleaned with the chisel. The risk of delayed hardening has to be considered; therefore, drilling into the mortar is avoided. Generally, one handful of mortar is sufficient for each sample. Of this, only a small percentage is analyzed; the rest is kept for mineralogical and chemical analyses, for archival use, and for any possible need to repeat the analysis. Details of the theoretical background for mortar hardening and dissolution, sample preparation techniques, and prescreening of samples to evaluate suitability for dating have been given previously (Lindroos et al. 2007).

For the <sup>14</sup>C measurements, accelerator mass spectrometry (AMS) is needed. The major advantage of AMS analysis over conventional <sup>14</sup>C measurement is that much smaller samples are required. Whereas a conventional measurement typically requires several grams of prepared carbon, AMS demands only a milligram or less. This allows higher selectivity in many small fractions and uniform acid dissolution reaction in small volumes. Our initial attempts of mortar dating with the conventional <sup>14</sup>C method (e.g. Ringbom and Remmer 1995; Ringbom et al. 1996) were sensitive to contamination, resulting in large scatter and too high ages. Thus, we now only rely on age determinations based on AMS.

### **METHODS**

We have focused our AMS measurements on well-defined concentrates of binder carbonates. Via mechanical separation we try to produce some hundreds of milligrams of powder that is homogenous with respect to both grain size and composition for AMS dating. The mortar sample is gently crushed—a process that preferentially breaks up the porous, soft mortar carbonate while leaving the harder limestone particles intact—and then sieved using increasingly fine mesh widths ranging between  $20{\text -}500\,\mu\text{m}$ . The grain-size fractions  $<100\,\mu\text{m}$  that may be used for dating are subsequently wet sieved. The small grains of mortar carbonate fragments pass through the coarser sieves and are thus separated from the large aggregate grains, including the calcite crystals of the unburned limestone. By wet sieving, the mortar carbonate is enriched to  $60{\text -}80\%$  in the fine grain-size windows extracted for dating (usually  $39{\text -}75$ ,  $39{\text -}62$ , or  $63{\text -}74\,\mu\text{m}$  depending on sample size and available sieves). Recently, we have mostly used  $46{\text -}75\,\mu\text{m}$ , whereas the content of limestone is typically reduced to less than 3%.

Following the mechanical separation, the mineral composition is analyzed by petrographic microscopy supplemented with cathodoluminescence, which helps to identify the contamination from aggregate limestone and marble (Lindroos et al. 2007 and references therein). Calcite of geological origin is usually, but not always, revealed as brilliant orange or red spots against the mortar binder carbonate, which forms a dull gray or brown background (Figure 2). Incompletely calcinated limestone residues are best identified microscopically in thin sections of mortar pieces where they show up as rusty lumps.

We have usually disqualified samples displaying abundant luminescent calcite or analyzed them only in order to get information about the nature of the contamination. In some cases, however, the contaminants are not luminescent, or they have lost their luminescence due to weathering, fire dam-

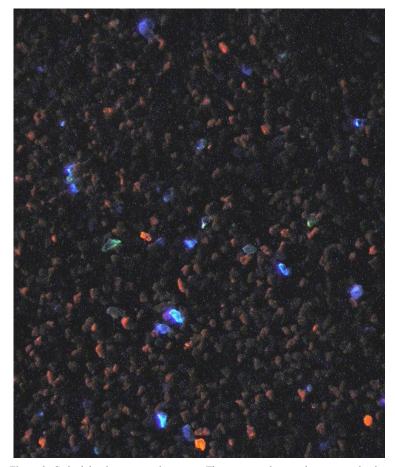


Figure 2 Cathodoluminescence microscopy. The orange-red spots show contaminating filler limestone, whereas the blue spots are quartz crystals without any significance for the dating analysis. Sample 146 from the church of Saltvik; 63–74μm grain-size fraction.

age, etc. The <sup>14</sup>C profiles (see below) themselves are therefore the most reliable and sensitive indicators of contamination.

In the chemical separation, 85% phosphoric acid is poured over the mortar powder under vacuum. In theory, mortar binder carbonate dissolves much easier than limestone. Thus, the process starts out with a violent reaction, liberating  $CO_2$  from the fast dissolution of the pure binder carbonate, and then the reaction gradually slows down, reflecting the slow dissolution of the remaining binder carbonate and the slowly dissolving sedimentary filler carbonates and unburned limestone from the quarry. Until about 2002, the emitted  $CO_2$  gas was collected cryogenically in 2 successive fractions, the first representing the gas evolved in less than 10 s and the second fraction the gas produced the following 20–40 min, respectively. Only these 2 fractions were dated while the remaining  $CO_2$  was not collected (nor measured). The age of the first  $CO_2$  fraction is assumed to be closer to the true date than that of the second fraction (Folk and Valastro 1976).

To gain more information on the dissolution process and the content and nature of contaminants, we started collecting typically 5 successive fractions to create age profiles of the samples. When the

acid is admitted to the sample, the reaction releases 10-20% of the total carbon dioxide in a matter of seconds. The evolved gas is quickly collected cryogenically in a glass vial as a first  $CO_2$  fraction. The reaction gradually slows down, and the second fraction comprising the next 10-20% is collected in a matter of minutes, while the subsequent fractions are reacted and collected sequentially in the order of hours (Figure 3). Since there is abundant mortar binder carbonate that is more readily soluble than limestone, the binder will be strongly represented in the carbon dioxide of the first  $CO_2$  fraction, which is assumed to be less affected by contamination from the slowly dissolving unburned limestone than subsequent fractions. Only in rare cases is the first fraction affected by too-young  $CO_2$  due to recrystallization or the building having been exposed to fire. This is revealed either in the chemical prescreening with phenolphthalein showing an alkaline reaction or by the age profile itself as discussed below. This method of chemical separation based on reaction rates works well for the Åland mortars, but elsewhere other methods like titration with diluted hydrochloric acid (HCl) have been tried, e.g. on Roman pozzolana mortars (Hodgins et al. 2010).

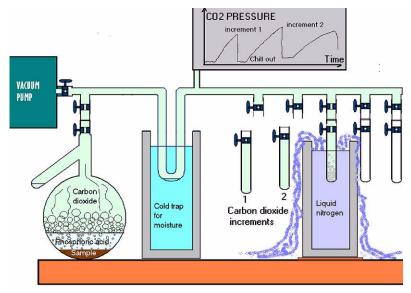


Figure 3 Chemical separation in  $5 \, \text{CO}_2$  fractions. The reaction has continued for some minutes and  $2 \, \text{CO}_2$  fractions have already been isolated. The third fraction is being chilled out cryogenically using liquid nitrogen.

### **AMS and Stable Isotope Measurements**

Part of the resulting  $CO_2$  gas was used for  $\delta^{13}C$  and  $\delta^{18}O$  analysis on a GV Instruments Isoprime stable isotope mass spectrometer to a precision of 0.15‰, while the rest was converted to graphite for AMS  $^{14}C$  measurements via reduction with  $H_2$  using cobalt as a catalyst (Vogel et al. 1984). Prior to laboratory number AAR-10100, stable isotope measurements were performed on the mass spectrometer at the Science Institute, Reykjavík. All AMS  $^{14}C$  measurements were carried out using the EN tandem accelerator at Aarhus University (Denmark). The dating results are reported according to international convention (Stuiver and Polach 1977) as conventional  $^{14}C$  dates in  $^{14}C$  yr BP (before AD 1950) based on the measured  $^{14}C/^{13}C$  ratio corrected for the natural isotopic fractionation by normalizing the result to the standard  $\delta^{13}C$  value of –25‰ PDB (Andersen et al. 1989). The conventional  $^{14}C$  dates were calibrated using the OxCal v 3.10 program (Bronk Ramsey 1995, 2001).

### The Aland Limestone and Mortar

The Åland Islands are a central part of the Scandinavian, Precambrian basement in northern Europe. The main island is composed of granites and the smaller islands to the west and south (Kumlinge, Föglö, and Kökar; Figure 13) of granites, gneisses, and schists. There are no marble quarries in the basement rocks in Åland, but they are common in the archipelago to the east, closer to the Finnish mainland. North of the islands, the bottom of the Baltic Sea is, however, covered with Ordovician limestone (Winterhalter et al. 1981) and the limestone has probably also covered the Åland Islands, but it has been eroded away during the glaciations. It can only be found at the bottom of Lumparn Bay, and as a major component in the loose overburden (the glacial till). It also occurs as abundant glacial blocks all over the area except for Kökar. It has different colors, reddish, yellowish, and different shades of gray and a benthic (organisms living on the sea floor) fauna with macrofossils. The mortar in the churches has been made by collecting and burning limestone blocks lying around in the terrain.

### Interpretation of Age Profiles

The well-preserved medieval mortars from the churches of the Åland Islands have had a central role in developing an AMS <sup>14</sup>C-based method for dating non-hydraulic mortars. The theoretical principles and several examples from the churches have been presented in Lindroos et al. (2007). That article is, however, addressed to the scientific community and it only discusses the interpretation of age profiles in several fractions, or the results obtained after 2002. This time, we present the entire corpus of the Åland results beginning from 1994 when we changed from conventional <sup>14</sup>C dating to <sup>14</sup>C AMS analysis, thus also including results analyzed in only 2 fractions between 1994 and 2002. The feedback we received from archaeologists is that our complex method should be presented in a more readable way so that those other than specialized scientists can also interpret the results and evaluate if a dating is reliable or not. We have therefore defined different reliability criteria based on our experience from Åland, Portugal, and Rome (Langley et al. 2010; Ringbom et al. 2010).

We have modeled the dissolution of limestone-based mortar as follows:

- 1. The binder is composed of 2 types of crystals: A, rapidly dissolving (sharp corners and edges of grains; lime-lump dust; well-developed, pure crystals). B, the remaining, impure cryptocrystalline to microcrystalline binder dissolving slowly.
- Very slowly dissolving contaminants of improperly burned limestone forming rusty lumps together with iron and manganese hydroxides. This component is responsible for the generally occurring increase in age at the end of the profile.
- 3. Sedimentary limestone grains originating from the filler. They dissolve slower than 1A but faster than 1B. This intermediate behavior creates a bump in the profiles. Figure 4 shows theoretical, modeled profiles including components 1–3.

When we consider these components and give numerical values to the dissolution rates, a typical mortar sample from Åland would yield profiles like the ones in Figure 4.

The distinction between aggregate limestone and improperly burned limestone residues is based on measured limestone dissolution rates (Lindroos 2005) and the stable isotope signatures ( $\delta^{13}$ C values in the Appendix). In dissolution tests, the Åland limestone dissolves relatively rapidly and as an Ordovician marine limestone; its  $\delta^{13}$ C value is near zero or slightly negative (according to a general Ordovician trend by Veizer et al. 1999; no measured values are available). The mortar binders tend to have  $\delta^{13}$ C values more negative than -7 (see Appendix). We interpret the commonly occurring, increased  $^{14}$ C ages and  $\delta^{13}$ C values for the second and third fractions as being due to aggregate lime-

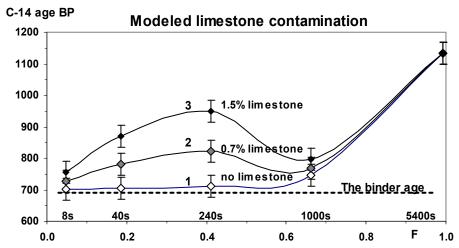


Figure 4 Modeled <sup>14</sup>C profiles showing the effect of typical limestone contamination. The sample age is set at 700 BP and 3 profiles were generated by modeling with 0%, 0.7%, and 1.5% filler limestone contamination, respectively. The dissolution progress F (from 0–1 or 0–100%) is shown as abscissa together with the dissolution time in seconds. The other parameters (30% rapidly dissolving binder, 68% slowly dissolving binder, and 1% unburned limestone residues) are kept constant. The increasing ages at the end of the profiles are due to the slowly dissolving limestone residues after incomplete calcination. The calculations are presented in Lindroos et al. (2007).

stone contamination. The fifth fractions have commonly increased  $^{14}C$  ages, but no clear correlation with the  $\delta^{13}C$  values. In some cases, the last fractions are the most negative ones and clearly not caused by limestone. We have reasoned that the last fractions are affected by unburned limestone residues. They dissolve slowly because they contain iron and magnesium hydroxides after thermal break-down of the iron and magnesium carbonate component of the limestone. The rather negative  $\delta^{13}C$  values may be due to several days of interaction with carbon dioxide and water vapor from wood during lime burning.

The shift in  $\delta^{13}$ C values has been used to estimate the amount of limestone contamination present in mortars (e.g. Van Strydonck et al. 1986; Ambers 1987). The Åland material is unsuitable for this kind of calculation (Lindroos et al. 2007). The main reasons are the broad spectrum of  $\delta^{13}$ C values for the binder carbonate within a sample, commonly occurring lime lumps with deviating values, and the lack of data for the limestone.

Practically all the Åland samples have turned out to yield curves resembling those of Figure 4, and the first fraction usually dates the time of hardening of the mortar (exceptions are fire-damaged mortars, where the first fraction is generally too young as discussed below). In Åland, where we know the dissolution behavior of the mortars, we would consider a profile resembling profile 1 in Figure 4 a successful dating giving a conclusive result. We define this type of result as Criterion I (CI):

### Criterion I

The  $^{14}$ C ages of the first 2 CO<sub>2</sub> fractions are the same (1 sample per building unit is in principle sufficient for a conclusive result).

The rationale behind this criterion is that if there is no age gradient (i.e. no increase in limestone contamination) from fraction 1 to fraction 2, then both fractions are most likely free of contamination and therefore date the time of hardening of the mortar. The quoted date of the mortar sample is based on fraction 1 only in order not to exaggerate the precision of the result.

Most profiles resemble profiles 2 and 3 (initial positive age gradient) in Figure 4. If the first fractions consistently yield the same age, we consider it a successful dating according to Criterion II (CII):

### Criterion II

Mutual agreement between the dates of the first  $CO_2$  fractions in a series of 3 or more samples from 1 single building unit.

The rationale behind this criterion is the following: Although the age gradient indicates a degree of contamination in fraction 2—and therefore possibly also in fraction 1—it is more likely that all first fractions have insignificant limestone contamination than all of them having the same amount of significant contamination, leading to the same age excess for all samples.

Many samples yield valuable data that are not sufficient for conclusive dating, but when put into a context it may help to clarify the chronology:

#### Criterion III

Mutual agreement between the dates of the first CO<sub>2</sub> fractions in 2 samples from 1 single building unit.

### Criterion IV

Where the first CO<sub>2</sub> fraction from 1 sample in a building unit yields a date that fits into a relative chronology.

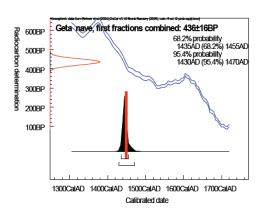
Below, we give some examples of the use of the criteria as well as a comparison with dendrochronology:

CI. The church of Geta provides an example of CI mortar dates, and attempts of dendrochronological dating have been published earlier (Ringbom et al. 2009). This church, originally a satellite chapel under the church of Finström, is also an example of how confusing the results of dendrochronology can be. Every second roof truss pointed towards the 1590s; the other half belonged to the 1820s—clearly a case of stepwise renewal of timber, possibly with none of the original remaining. Only 1 timber log, a wall plate integrated in the wall, appeared to be part of the original, medieval construction. It was felled some time shortly after 1450. In this case, mortar dating was the only possible way to resolve the chronology.

In this case, 3 age profiles of mortars from the nave provided reliable CI dates (Figure 5) and one of them is especially reliable because it shows no limestone contamination at all. The combined calibration of the first CO<sub>2</sub> fractions suggests the age AD 1435–1455, in excellent agreement with the dendrochronological date of the wall plate (Figure 5, top right). This result is further supported by the <sup>14</sup>C age of a wooden fragment encapsulated in the mortar giving a minimum age. Mortar dating solved the riddle of the dendrochronology results: the medieval wall plate does indeed reflect the age of the nave of the church in Geta.

CII. The 4 mortar age profiles from the nave of the church of Finström represent a CII case (Figure 6). This church is one of the best preserved medieval buildings in Finland. This is true of both the exterior and the interior and the decorative program. Many different indications suggest that it must have been one of the most important—and therefore early—churches in the Åland Islands, with close connections to the Diocese in Turku (mainland Finland). Yet, this church has an incredibly confusing building history. Remains of a wooden predecessor on the site have been excavated archaeologically. It probably dates from the end of the 12th century, whereas dendrochronology on the present church points towards a substantial rebuilding of the stone church in the mid-15th century, cf. other interpretations (Sárkány 1973; Dreijer 1983:307–16; Hiekkanen 2007:366–71).





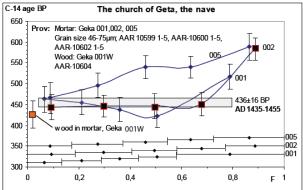


Figure 5 The church of Geta with 3 age profiles from mortar analysis and 1 dating of a wooden chip within one of the mortar samples. The size of respective  $CO_2$  fraction is marked at the bottom of the plot. The combined calibration of the first  $CO_2$  fractions yield AD 1435–1455 (top right panel), in excellent agreement with the dendro date (vertical line) of roof timber integrated in the wall. The age profile for Geka 002 (marked with large, square symbols) is very similar to profile 1 in Figure 4, making it especially reliable and a clear CI case. The 2 other samples also belong to CI because the first and the second fraction have overlapping ages. The mortar dating is further supported by the  $^{14}C$  age of a wooden chip enclosed in the mortar 001.

Dendrochronological analysis of the timber provides clear results for the different building units. Oldest is the sacristy from the AD 1440s, followed by the nave ~1450, the porch in the 1450s, and the tower in 1467. This late medieval age for the entire building was most surprising, and therefore, a number of mortar samples from the nave were taken to test whether the dendrochronological results really represent the age of the stone structures.

From a technical point of view, the lime of the mortar was well burned and has only little limestone contamination. The scarcity of unburned limestone residues is indicated by moderate or insignificant increase in ages for the fifth fractions. On the other hand, the significant bump in the mid-section of the age profile for sample Fika 058 indicates a non-negligible amount of limestone contamination in the filler. One of the age profiles, Fika 060, is almost horizontal, and completely devoid of contamination. The timber wood sample (Fika 060W) fits into the picture, with the highest probability AD 1440–1520. This is an example where 3 of the age profiles classify as CI, whereas they all 4 together represent CII. The first fractions thus provide a highly conclusive mortar date of AD 1440–1465, in perfect agreement with dendrochronology (~AD 1450) for the nave (Figure 6, top right, and Figure 12a).

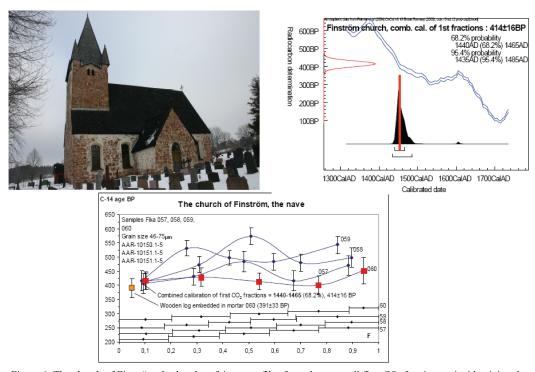


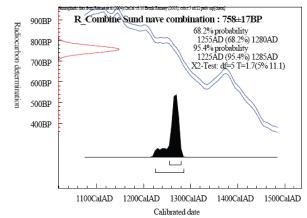
Figure 6 The church of Finström. In the plot of 4 age profiles from the nave, all first  $CO_2$  fractions coincide giving the weighted average age of  $414 \pm 16$  BP. The calibrated combined age probability distribution, AD 1440–1465 (top right panel) is completely consistent with the date suggested by dendrochronology of the nave, i.e. AD 1450 (vertical line; see also Figure 12a).

**Atypical profiles: fire damage.** The church of Sund is the largest among the Åland churches. There are, unfortunately, no results from dendrochronology available for this church. All datable wood from the nave has been consumed by several severe fires. The only surviving wooden samples were a couple of charred fragments of scaffolding and from a cast form in the staircase of the tower. They were also <sup>14</sup>C analyzed (cf. Figure 12c).

Thus, to determine the age of the nave, <sup>14</sup>C AMS analysis of scorched mortar was the only option. From the nave, including the vault, there are 5 age profiles, all of them behaving radically different from all other Åland samples. Two of the age profiles (Figure 7) have been presented in Lindroos et al. (2007). They may be considered special cases of fire-damaged mortars where a horizontal plateau in the middle of the profile corresponds to the archaeological age. The combined calibration of the plateaus yields AD 1255–1280, indicating that the nave of the church of Sund may be coeval with the early stages of all the other churches of the main island of Åland.

Naturally, these atypical age profiles have to be interpreted critically and with care, especially in the absence of age control. Yet, our recent research from other fire-damaged constructions, where there is age control, support our theory that burned mortars reach the correct age in later fractions of the age profile, whereas the early fractions from fast-reacting mortar carbonate appear young, reflecting recrystallization or conversion to active lime due to fire. Our experience from Sund has given important insights into identifying, interpreting, and dating buildings that have been devastated by fire. We have noted that age profiles from fire-damaged mortars that form clear plateaus seem to be





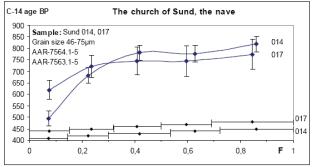


Figure 7 The church of Sund. Two age profiles of fire damaged mortar from the nave, both with mutually agreeing horizontal plateaus in the middle of the profiles. The plateaus are well-defined because they represent more than 50% of the CO<sub>2</sub> from each sample. A combined calibration of the fractions defining the plateaus yields a date of AD 1255–1280.

conclusive and reliable. These samples are therefore included as conclusive in the statistics. However, we still need further confirmation before we can state it as a fact.

### **RESULTS**

All the results for mortar samples dated in age profiles of 2-5 CO $_2$  fractions are given for each building unit in the Appendix along with  $^{14}$ C dates on wood and charcoal samples as well as summary dendrochronological dates. To begin with, in 1991–1992, dendrochronological analysis was applied wherever possible. Of the 283 total samples, 159 were conclusive. Some 107 were of medieval origin. The rest were inconclusive, either because the timber used was spruce, which cannot be dated satisfactorily, or because the annual rings were too few to establish a date matching to the master curve.

Dendrochronological dates have been published (Ringbom and Remmer 1995, 2000, 2005; Ringbom et al. 2009). Even though dendrochronology could not resolve the chronology of the earliest building stages, it generally provided firm datings for later building stages, and has thus been an important key to validation of mortar dating.

The strategy from the beginning of the project has been to test mortar dating on as many samples as possible against the dendrochronological age of the structure. There are altogether 38 mortar results that can be compared to dendrochronology. Where the calibrated <sup>14</sup>C dates are imprecise, for

instance in the 14th century where one can only identify the right century, dendrochronology often provides the much needed precision. Thus, the 2 methods are complementary. Dendrochronology gives the precise age and mortar dating confirms that it is relevant for the building phase we want to date. In Figure 8, we present calibrated <sup>14</sup>C age probability distributions of the mortar dates compared with the dendrochronological dates.

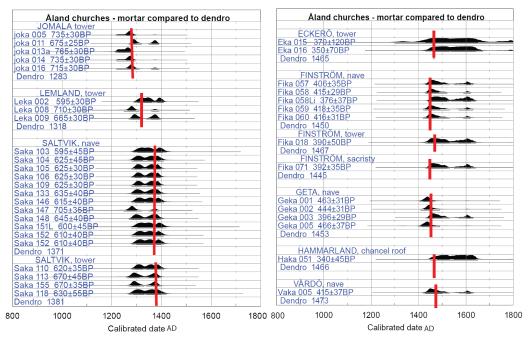


Figure 8 CI and CII Åland mortars (calibrated dates of the first  $CO_2$  fractions in black, presented horizontally) from a number of structures compared with the dendrochronologically determined age of the structures (vertical lines). Samples denoted Saka 151L and Fika 058Li are lime lumps from mortar samples with the same number.

Although many of the distributions are bimodal and do not point to an unambiguous date, the agreement is excellent. Thus, among 38 mortar samples dated by their first fractions according to CI and CII, 36 were found consistent at the 68.2% probability level with age control from dendrochronology.

However, it is possible to provide a more direct, unambiguous test of the reliability of the method of mortar dating, i.e. the assumption that it is possible to isolate and date a homogenous binder concentrate of the mortar sample, the  $^{14}$ C content of which reflects the atmospheric content at the time of the mortar hardening. Figure 9 shows all the conventional  $^{14}$ C dates plotted against their known calendar ages obtained from dendrochronology. The agreement of the  $^{14}$ C dates with the atmospheric calibration curve shown for reference is impressive, as more than 68% of the  $^{14}$ C results deviate less than 1  $\sigma$  from the atmospheric value.

We have analyzed a total of 150 mortar samples (Figure 10). In many cases, the mortars were in contact with wood that could not be dendrochronologically dated but <sup>14</sup>C dating was possible. When we include these in our database, we have 79 dated mortar samples with age control. For reasons not understood, 4 of them failed, yielding a deviating (older) age even if their age profiles look like CI samples. Some 75 mortar samples with age control proved to be conclusive and accurate within the measuring precision. The corresponding failure rate is thus ~5%. The remaining 71 samples had unknown ages, i.e. no independent age control. The reliability criteria were applied to these samples.

# 1000 14C dates on mortar 14C calibration curve 1998 800 14C age BP 600 > 68% within 1 sigma 400 200 1250 1300 1350 1400 1450 1500 Calendar age AD (dendro)

### All Åland mortar 14C dates with dendro age control

Figure 9 All Åland mortar samples with calendar ages known from dendrochronology. The conventional, uncalibrated mortar <sup>14</sup>C dates are plotted against the corresponding dendro age. Data points of the same calendar age are shown with slight x-offsets to allow distinction between points. The atmospheric calibration curve is shown for reference.

A majority (45) meet the requirements of CI and/or CII and we therefore regard these as successfully and firmly dated samples. These are our most important results, since they show the real potential of the mortar dating method. Here, mortar dating was the only option, and yet the results are conclusive. Based on our results for samples with age control, we expect the failure rate to be only about 5% for samples satisfying CI and/or CII and not exhibiting atypical age profiles. The 26 samples to the very right in Figure 10 are inconclusive, but for reasons well known. They have therefore been helpful in the development of the method. Some of them yield ages for the first CO<sub>2</sub> fractions that fit into the context provided by the other samples, but there are too few samples per unit (<3) to qualify for CII. That is, at least 3 samples should be dated from each building unit. In some cases, there are abnormal age profiles that we have not tried to interpret. Among them are several samples from the burned Sund church with inconsistent first CO<sub>2</sub> fractions and no clear age plateau in the mid-section of the profile.

### The Chronology of the Aland Churches

In Figure 11a–d, we present all the conclusive datings including dendrochronology and <sup>14</sup>C results from wood (see Appendix). Those in black denote calibrated ages of mortar dates. In all cases, except for the church of Sund and the east gable of Kumlinge, we have used the dates of the first CO<sub>2</sub> fractions. In yellow are the calibrated results of <sup>14</sup>C analysis of wood embedded in the mortar, or from fragments of wood, not well enough preserved for dendrochronology. Dendrochronological results are indicated by vertical lines in red.

## Age control, 79 samples

# No age control, 71 samples

75 samples agree with age control

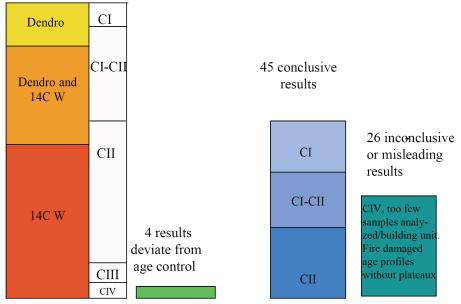


Figure 10 Classification of non-hydraulic samples from Åland. The stacks to the left in different colors (shades of gray), yellow (top), orange and red (bottom) include samples with an age control based on dendrochronology and/or <sup>14</sup>C-dated wooden structures. Some 75 samples out of a total of 79 agree with the known age. Four samples (second stack, in green) yielded deviating ages. The 2 stacks to the right show the datings without age control. The third stack in different shades of blue represents samples that yield results corresponding to CI and CII. They are our most important samples, providing successful and conclusive results where mortar was the only datable material available. The remaining 26 samples of unknown age remain inconclusive (far right), for reasons well understood.

Wherever there is age control, one can note a good agreement between wood and mortar. In rare cases, the wooden samples give a different age. They can be significantly older (Eka 007W, Haka 024W), or only a little older (Fika 018W, Fika 21W and Fika 063W). In case the odd wooden sample among otherwise homogenous results is younger (Eka 18W), one can suspect secondary replacements. In 2 cases, the mortar has yielded significantly older results (Haka 047 and Haka 045). Together with Leka 009 and Leka 008, they belong to those 4 that disagree with age control. Note further that dendrochronology, whenever it is available for a respective building unit, coincides with both the mortar and <sup>14</sup>C analysis of wood. In Hammarland, dendrochronology of the nave dates the rebuilding in the AD 1440s, after a fire, and is therefore not included in the diagram.

This comparison does not include <sup>14</sup>C analysis of charcoal embedded in the mortar, because it is generally too old. It yields uneven results, thus reflecting the "old wood effect." This is due to the fact that countless annual rings have burnt away in the fire, and the inner core often represents the only remains of the timber in questions. Charcoal has been systematically tested and analyzed for reference. By chance, the charcoal can yield an age identical to the mortar, but obviously it should not be younger than the mortar (charcoal dates are included in the Appendix).

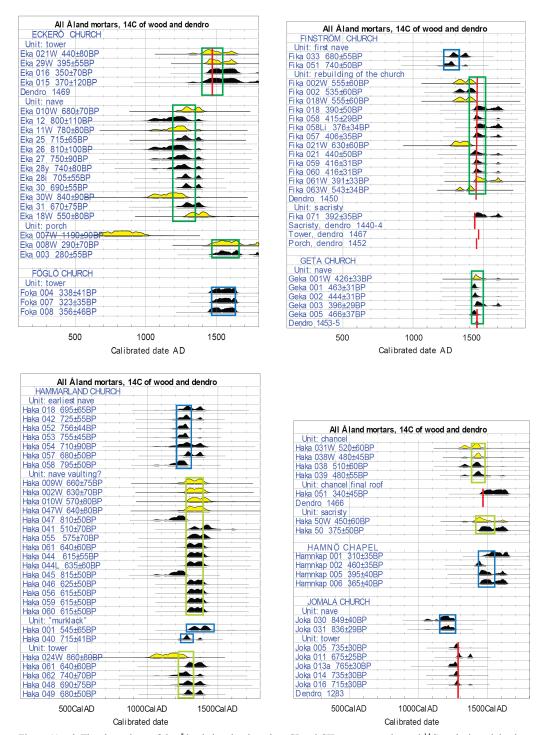
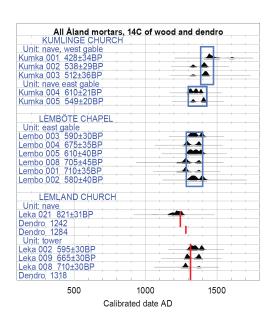
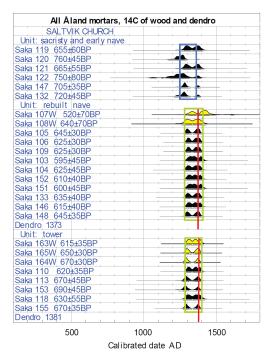


Figure 11a–d The chronology of the Åland churches based on CI and CII mortar samples and <sup>14</sup>C analysis and dendrochronology of preserved wood. Calibrated results of wood (W after ID number) are marked in yellow, mortar in black, and results of dendrochronology are indicated by a red vertical line. Framing rectangles in green mark the ages for different building units where the age is determined by mortar and <sup>14</sup>C of wood. Rectangles in blue present the age for building units where mortar has been the only dateable material.





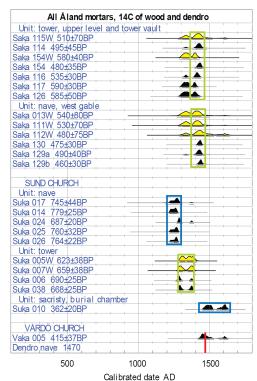


Figure 11a-d (Continued)

The green rectangles surrounding the samples of separate building units show the date suggested by mortar dating and age control from <sup>14</sup>C analysis of wood and dendrochronology. And, most importantly, the rectangles in blue show the result of building units where mortar has been the only option for scientific dating.

Considering the large amount of data and the fact that the mortar samples from Åland behave in a predictable way, we dare claim that the chronology of the Åland churches is taking shape (Figure 12a–b, cf. Figures 11a–d and Figure 13). It is noteworthy that the chronology basically remains the same, whether it is based on mortar dating or on scientific dating of wood. But once more it has to be stressed that mortar dating often is the only way to confine the time of the earliest building stages. We can see that the building activity is spreading rather uniformly from the end of the 13th century to the end of the Middle Ages.

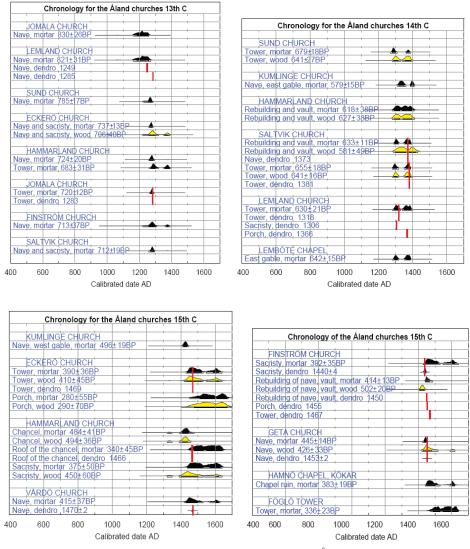


Figure 12a-b The compiled chronology for the medieval stone churches in Åland, presented century by century from the 13th to the 15th century. It is based on different science-based dating methods: <sup>14</sup>C AMS analysis of samples of mortar and wood (conclusive dates combined in each category), as well as results from dendrochronology.

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The main churches, or the mother churches, on the main island in Sund, Jomala, Eckerö, Hammarland, Saltvik, and Lemland (Figure 13), were all erected during the 13th century. The same age is indicated also at Finström, from a couple of preliminary mortar sample analyses from the foundation level of the nave (Figure 11a). It is therefore conceivable that an early stone church did exist in Finström, but both the plan and exterior so far remain unknown. These early dates often rely on mortar dating alone, on results that fulfill the demands of CI or CII, often a combination of both. Still, for the early naves in Jomala, Lemland, and Finström, it is our intention to have more samples analyzed. Lemland has the only 13th century nave dated by dendrochronology, and Jomala has the only church tower from that century.

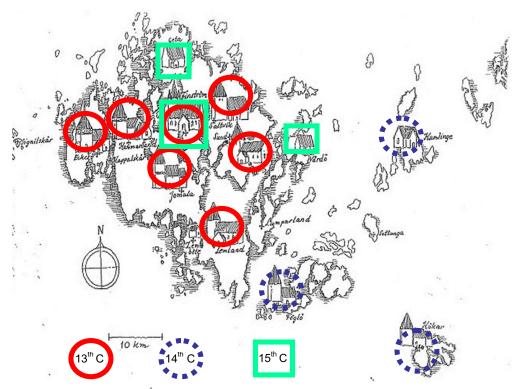


Figure 13 Chronology of the Åland churches

The chronology of the 14th century is not yet complete. As is well known, it is a century that is not easily defined by <sup>14</sup>C dating. Due to the irregular calibration curve, the timing so far remains unresolved. The century is remarkable for its many church towers and other secondary building units as sacristies and porches. Radical rebuilding and vaulting takes place in Saltvik at the end of the century, and these events are firmly dated by mortar dating and dendrochronology. The chapel of Lemböte, by the old sailing route from Denmark to Estonia, was either built at the end of the 13th century or in the 14th century. We have the age of the nave in Kumlinge fairly well established despite the fire-damaged mortars. The church on the remote island of Kökar will require additional consideration because the mortar is not necessarily made of the Åland limestone. Several different indications (archaeological artifacts, preliminary results, etc.) suggest that this church also may belong to the 14th century, as may also the church in Föglö.

The 15th century is a third dynamic building period in the Åland Islands. We have established evidence of a more or less total rebuilding of the stone church in Finström. Here, the dendrochronology suggested new roofs in the nave and sacristy. It also marked the erection of a porch and an impressive new tower. The mortar, sampled from a wide area around the roof construction, confirms that the dendrochronology actually marks a wider rebuilding of the entire church. It also involved the vaulting and the heightening of the nave. Three more towers were erected this late, in Eckerö, Föglö, and Kumlinge. Completely new constructions were the satellite churches, or the chapels of Geta and Vårdö, administered by Finström and Sund, respectively. Surprisingly enough, it seems that the little wooden chapel "Kappalskatan" in Hamnö, Kökar, belongs to the very end of this building period. No wood remained for analysis, but mortar from the foundation level indicates that this may be the most recent medieval ecclesiastic building in Åland, from the very beginning of the 16th century.

However, to get the full picture of the chronology of the Åland churches, it may be useful to compare Figure 12 with the map of the Åland churches, where the different ages of the naves are marked in different colors (Figure 13). It is obvious that the 13th century is the most dynamic period in the islands, with 7 mother churches (marked in red) erected close together on the main island. The 14th century meant new churches in the archipelago (marked in dotted blue circles). On the main island, it was only a matter of adding secondary building units to existing naves.

The 15th century appears strongly represented in Figure 12b. However, it looks different when it comes to the bigger building projects (Figure 13). Apart from the remarkable rebuilding of Finström, it really only involves the erection of 2 new satellite chapels, Geta and Vårdö, plus innumerable secondary building units added to earlier naves.

Our work on <sup>14</sup>C mortar dating has been consistently criticized since 1994 by one author, who specializes in medieval stone churches in Finland (Hiekkanen 1994, 1998, 2004, 2007, 2008, 2009). This author believes that the mortar-dating approach cannot be used for dating these materials.

### CONCLUSIONS

In conclusion, Åland mortars have turned out to be exceptionally "well behaved" and well suited for  $^{14}$ C dating compared to samples from our later studies of mortars from ancient Rome. Analyzed in 2 or more  $CO_2$  fractions, the results of the first  $CO_2$  fractions are simple to interpret and yield unambiguous dates:

- It was fortunate that our systematic development of mortar dating was initiated in the Åland Islands, where the non-hydraulic lime mortar is well-preserved and behaves in a predictable way in phosphoric acid hydrolysis and where there is plenty of feedback available from age control of dendrochronology and AMS <sup>14</sup>C analysis of wood.
- Mortar dating is often the only way to determine the age of the first building stage of the churches. Without mortar dating, the chronology of the Åland churches could not have been established.
- Wherever age control has been available, 95% of all mortar sample dates are correct.
- Of all the 150 samples analyzed, 80% are conclusive (that is, they either agree with age control or satisfy CI and/or CII).
- Churches devastated by fire have mortars that yield atypical <sup>14</sup>C profiles.
- While petrographic microscopy and cathodoluminescence are useful for a crude screening against mortar samples that are unsuited for <sup>14</sup>C dating, the <sup>14</sup>C profiles are the most reliable and sensitive indicators of possible dating errors due to contamination.

For the future, it is our aim to map areas where mortar dating is feasible. From our vast experience of dating 444 mortar samples from all over Europe, from classical antiquity to Post-Reformation times, from different parts of the Roman Empire to different parts of Scandinavia, we can already now say that non-hydraulic lime mortars seem to be easier to analyze than hydraulic mortars. Our reliability criteria work also outside the Åland Islands, but we still have to find out how universally they can be applied. In cases when they may not work, we will have to find out why. We will have to compare results from parallel testing of hydrochloric acid and phosphoric acid in the chemical separation, and find out if they behave differently in different geological terrains.

### **ACKNOWLEDGMENTS**

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### **APPENDIX**

Dated mortar samples and fractions along with comparative dates on wood and charcoal as well as dendro dates. Those  $CO_2$  fractions that date the samples according to criteria discussed in the text are emphasized in **boldface**, while wood and charcoal samples that are clearly not associated with the time of hardening of the mortar are given in *italics*. Misleading or inconclusive mortar samples are also given in italics. Laboratory numbers are Aarhus AAR numbers unless otherwise indicated (Hel-# are Helsinki conventional Radiocarbon Laboratory). Where only estimates are available,  $\delta^{13}C$  values are given in square brackets. Grain-size fractions that have not been recorded are marked NR.

Appendix	Dated morta	l samples and	fractions.
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	Lab nr		C yield (%);		<sup>14</sup> C		$\delta^{13}C$	$\delta^{18}O$		
	Aarhus		grain-size	Fraction		±	<b>‰</b>	<b>‰</b>		
Sample	(AAR-#)	Type	fraction (µm)	size (%)	(BP)	1 σ	VPDB	VPDB	Criteria	Comments
ECKERÖ CHU	RCH									
Unit: tower (cor	nclusive)									
Eka 021	1474	plant			440	80	-28.5			
EKA 029W	2001	wood			395		-23.4			
Eka 015	1471.1	mortar	3.8; NR	45	370		<b>-11.7</b>	-17.3	CI	
Eka 015	1471.2	mortar		55	390		-11.5	-18.6		
Eka 016	1472.1	mortar	5.2; NR	48	350		-10.4	-19.9	CIII	
Eka 016	1472.2	mortar		52	570	70	-8.6	-20.9		
Dendro: AD 146										
Unit: nave (cond										
Eka 010W	Hel-2999	wood			680	70			ST ST	
Eka 012	1470.1	mortar	6.2; NR	40	800		-15.7	-22.4	CI, CII	
Eka 012	1470.2	mortar		60	855	65	-8.9	-21.4		
Eka 011W	Hel-3000	wood	0 ( (2 = 1	••	780	80	42.2	40.0	OI OII	
EKA 025.1	2062.1	mortar	8.6; 63–74	29	715		-13.3	-13.3	CI, CII	
EKA 025.2	2062.2	mortar	-0 (2 -1	71	790		-11.1	-11.1	OI OII	
EKA 026.1	2063.1	mortar	5.8; 63–74	43	810		-16.1	-22.7	CI, CII	
EKA 026.2	2063.2	mortar	- 4 62 - 4	57	850		-14.6	-22.5	CIT	
EKA 027.1	2064.1	mortar	5.4; 63–74	46	750		-11.5	-19.2	CII	
EKA 027.2	2064.2	mortar	40 56 405	54	1040		-10.9	-19.2	CIT	
Eka 027-2.1	2064-2.1	mortar	4.8; 76–125	19.2	855		-12.64	-19.57	CII	
Eka 027-2.2	2064-2.2	mortar		18.4	965		[-9]	10.00		
Eka 027-2.3	2064-2.3	mortar		19.0	1076		-11.29	-19.82		
Eka 027-2.4	2064-2.4	mortar		17.7	1149		-11.37	-19.87		
Eka 027-2.5	2064-2.5	mortar		24.4	1801		-10.96	-19.82		
EKA 028 C	2000	charcoal		22	640		-24.2	10.6	CII	
EKA 028i.1	2065.1	mortar	8.1; 63–74	32	740		-13.6	<b>-19.6</b>	CII	
EKA 028i.2	2065.2	mortar	(7. (2.74	68 <b>34</b>	1010	55		-17.8	CII	
EKA 028y.1	<b>2066.1</b> 2066.2	mortar	6.7; 63–74	<b>54</b> 66	<b>705</b> 1260		<b>−13.3</b> −10	<b>−20.4</b> −19.9	CII	
EKA 028y.2 EKA 030 W	2049	mortar wood		00	840		-24.2	-19.9		
	2049 2067.1		7.3; 63–74	33	690		-24.2 - <b>18.5</b>	10.0	CI, CII	
EKA 030.1 EKA 030.2	2067.1	mortar mortar	7.3; 03-74	<b>67</b>	690		-1 <b>3.</b> 3	<b>−19.9</b> −17.3	CI, CII	
Eka 030-2.1	2067.2 2067-2.2.1		7.7; 63–74	22.1	[7 <b>05</b> ]		-13.3 - <b>19.64</b>	-17.3 - <b>19.94</b>	CI, CII	
Eka 030-2.1 Eka 030-2.2	2067-2.2.1		7.7, 03-74	17.3	889	33	-7.73	-19 <b>.94</b> -14.94	CI, CII	
Eka 030-2.2 Eka 030-2.3	2067-2.2.2			23.9	955	11	-7.73 $-14.62$	-14.94 $-17.89$		
Eka 030-2.3 Eka 030-2.4	2067-2.2.3			19.3	895		-14.02 $-15.42$	-17.89 $-17.39$		
Eka 030-2.4 Eka 030-2.5	2067-2.2.4			38.2	1200		-13.42 [-15]	-17.39		
EKA 030-2.3 EKA 031.1	2067-2.2.3 2068.1	mortar	6.0; 63–74	36.2 <b>40</b>	670		[-13] - <b>11.4</b>	-20.1	CI, CII	
EKA 031.1 EKA 031.2	2068.2	mortar	0.0, 05-74	60	670		-11.4 -12	-20.1 -22.1	CI, CII	
Eka 018W	Hel-3002	wood		50	550	80		-22.1		
Unit: porch (con		woou			550	00				
Eka 007W	Hel-2997	wood			1190	90				
LIM UU/II	1101-477/	woou			1170	20				

Appendix	Dated mortal samples and fractions.	(Continued)
rppenan	Buteu mortar sumpres una muenons.	(Communica)

Appendix Dated in	iortai sampie	s and maci	nons. (Continue	α)						
	Lab nr		C yield (%);		$^{14}C$		$\delta^{13}C$	$\delta^{18}O$		
	Aarhus		grain-size	Fraction	age	$\pm$	<b>‰</b>	<b>‰</b>		
Sample	(AAR-#)	Type	fraction (µm)	size (%)	_	1 σ	VPDB	VPDB	Criteria	Comments
Eka 008W	Hel-2998	wood	. ,	/	290	70				
Eka 003.1	1469.1	mortar	7.4; NR	35	280	55	-13		CI	
Eka 003.1 Eka 003.2	1469.2	mortar	7. <b>4</b> , 1111	65	210	70	-10.4	-18.9	CI	
LK4 003.2	1407.2	mortai		03	210	70	-10.4	-10.7		
FINSTRÖM CHU	URCH									
Unit: first nave (c										
Fika 033.1	1877.1	mortar	4.8, <250	32	680	55	-13.4	-15.1	CI, CIII	
			panned						,	
FIKA-033.2	1877.2	mortar		68	760	60	-8.7	-13.1		
Fika 050.1	8952.1	mortar	4.7; 76–150	19.9	505	47	-20.64	-16.56	test .	from deep
									sample	within wall, i.e.
										delayed hard- ening, and very
										negative $\delta^{13}$ C
Fika 050.2	8952.2	mortar		19.6	660	60	-19.87	-21.66		S
Fika 050.3	8952.3	mortar		19.4	667	45	-22.02	-24.41		
Fika 050.4	8952.4	mortar		18.4	592	47	-21.81	-23.88		
Fika 050.5	8952.5	mortar		22.3	740	90	-21.7	-24.83		
Fika 051-2.1	8953-2.1	mortar	6.4; 76–150	15.7	740	50	-19.82	-20.08	CI, CIII	
Fika 051-2.2	8953-2.2	mortar		17.3	687	48	-17.34	-20.4		
Fika 051-2.3	8953-2.3	mortar		15.3	712	47	-18.66	-21.02		
Fika 051-2.4	8953-2.4	mortar		14.9	675	70	-19.4	-22.58		
Fika 051-2.5	8953-2.5	mortar		37.3	738	47	-19.26	-23.48		
Unit: rebuilding of	,		4.0.76.150	10.7	406	42	11 40	12.16		
Fika 052.1	8954.1	mortar	4.0; 76–150	19.7	496	43	-11.49	-13.16		
Fika 052.2	8954.2	mortar		21.6 20.3	450 515	65 75	-12.67 $-13.31$	-15.08		
Fika 052.3 Fika 052.4	8954.3 8954.4	mortar mortar		12.2	500	50	-13.31 -13.37	-16.12 $-16.67$		
Fika 052.4 Fika 052.5	8954.5	mortar		26.8	553	50	-13.37 -13.2	-17.28		
Fika 002.1	1862.1	mortar	8.8; <250	25.6 25	535	60	-13.2 -13.7	-17.26 - <b>18.4</b>	CI, CII	
1 IKa 002.1	1002.1	mortar	panned	23	353	00	10.7	10.4	CI, CII	
Fika 002.2	1862.2	mortar		75	375	45	-9.6	-16.8		
Fika 002W	1863	wood			555	60	-24.2			
Fika 018.1	1864.1	mortar	8.5; <250	33	390	50	-11.8	-20.2	CI, CII	
			panned							
Fika 018.2	1864.2	mortar		67	470	60	-9.2	-19		
Fika 018W	1865	wood	- 4 46	•••	555	65	-20.3	40.04	OT OT	
Fika 058.1	10151.1	mortar	7.1; 46–75	20.7	415	29	-10.51	<b>-19.01</b>	CI, CII	
Fika 058.2	10151.2	mortar		20.4	473	28	-10.01	-18.74		
Fika 058.3	10151.3	mortar		19.5 18.8	574 480	29	-10.86 $-10.74$	-20.67		
Fika 058.4 Fika 058.5	10151.4 10151.5	mortar mortar		20.7	480	30 35	-10.74 -11.88	-21.09 -21.41		
Fika 058Li.1	10151.5 10155.1	lime	5.3; 21–150	75	<b>376</b>	34	-11.88 - <b>7.04</b>	-21.41 - <b>19.31</b>	CI, CII	
Fika 058Li.1	10155.1	lime	5.5, 21-150	25	439	39	-7. <b>04</b> -8.14	-21.29	CI, CH	
Fika 057.1	10150.1	mortar	6.7; 46–75	18.9	406	35	-10.5	-18.68	CI, CII	
Fika 057.2	10150.2	mortar	,	19.6	431		-10.4	-18.85	,	
Fika 057.3	10150.3	mortar		19.4	485	37	-11.21	-20.52		
Fika 057.4	10150.4	mortar		18.9	417	35	-11.68	-21.08		
Fika 057.5	10150.5	mortar		23.2	470	34	-11.23	-21.85		
Fika 021.1	1866.1	mortar	6.3; <250	50	440	50	-12.1	-19.1	CI, CII	
			panned			_				
Fika 021.2	1866.2	mortar	ND NO	50	470	50	-11.3	-18.3	CIT	
Fika 021	1867	lime	NR; NR		400	55	-7.4		CII	
Fika 021W	1878	wood			630	60	-24.1			
Fika 022W	1868	wood	(7.46.75	17.6	405	55 35	-24.3	20.27	CII	
Fika 059.1	10152.1	mortar	6.7; 46–75	17.6	416	35	-17.59	<b>-20.37</b>	CII	
Fika 059.2	10152.2	mortar		16.7	531 498	28 26	-9.46 $-13.02$	-16.57		
Fika 059.3	10152.3	mortar		16.6	498	∠0	-15.02	-18.76		

	Lab nr		C yield (%);		$^{14}C$		$\delta^{13}C$	$\delta^{18}O$		
	Aarhus		grain-size	Fraction	age	±	<b>‰</b>	<b>‰</b>		
Sample	(AAR-#)	Type	fraction (µm)	size (%)		1 σ	VPDB	VPDB	Criteria	Comments
Fika 059.4	10152.4	mortar		17.4	484	30	-13.86	-19.54		
Fika 059.5	10152.5	mortar		31.8	544	31	-13.47	-19.59		
Fika 060.1	10153.1	mortar	6.7; 46–75	20.5	416	31	-11.97	-19.21	CI, CII	
Fika 060.2	10153.2	mortar		22.5	430	33	-6.2	-16.9		
Fika 060.3	10153.3	mortar		22.1	414	29	-9.25	-18.87		
Fika 060.4	10153.4	mortar		23.4	401	32	-10.07	-19.06		
Fika 060.5	10153.5	mortar		11.5	453	46	-10.88	-19.29		
Fika 061W	10156	wood			391	33	-25.5			
Fika 063W	10157	wood			543	34	-24.73			
Unit: sacristy										
Fika 071.1	10154.1	mortar	7.8; 46–75	23	392	35	-16.27	-18.62	CI	
Fika 071.2	10154.2	mortar	,	21	432	38	-9.4	-15.99		
Fika 071.3	10154.3	mortar		20.2	398	43	-12.8	-17.32		
Fika 071.4	10154.4	mortar		19.8	350	36	-13.96	-17.83		
Fika 071.5	10154.5	mortar		16	589	32	-13.85	-17.51		
Dendro: AD 1440										
Unit: tower	1									
Dendro: AD 1467										
Unit: porch										
Dendro: AD 1452										
EÖGLÖ GUUDA	711									
FÖGLÖ CHURC Unit: nave (incon										
Foka 001.1	11855.1	mortar	8.4; 46–75	12.7	393	34	-21.95	-20.48	incon- clusive	too recent, sec- ondary repair?
Foka 001.2	11855.2	mortar		20.4	571	32	-11.01	-17.89	ciusive	ondary repair.
Foka 001.2	11855.3	mortar		22.6	760	39	-12.26	-19.15		
Foka 003.1	11857.1	mortar	8.8; 46–75	10.8	610	31	-20.67	-20.72	CIV	too few sam- ples analyzed
Foka 003.2	11857.2	mortar		23	714	28	-8.84	-18.6		pies anaryzeu
Foka 003.3	11857.3	mortar		21.3	1085	46	-9.88	-19.29		
Unit: tower (cond	clusive)									
Foka 004.1	12323.1	mortar	8.3; 46-75	9.1	338	41	-26.36	-14.86	CII	
Foka 004.2	12323.2	mortar	,	19.7	446	30	-13.49	-15.42		
Foka 004.3	12323.3	mortar		18.0	636	33	-13.71	-15.6		
Foka 006.1	12324.1	mortar	8.0; 46–75	9.1	475	35	-26.05	-19.26	incon- clusive	
T 1 006 2	100040			20.0	500	2.5		15.45	ciusive	

									ciusive
Foka 006.2	12324.2	mortar		20.0	589	35	-11.44	-17.47	
Foka 006.3	12324.3	mortar		18.1	694	44	-10.67	-17.57	
Foka 007.1	12325.1	mortar	7.6; 46–75	9.3	323	35	-20.43	-19.89	CII
Foka 007.2	12325.2	mortar		20.2	493	36	-6.93	-17.58	
Foka 007.3	12325.3	mortar		19.3	481	34	-9.19	-18.71	
Foka 008.1	12326.1	mortar	6.7; 46–75	9.7	356	47	-22.7	-18.16	CII
Foka 008.2	12326.2	mortar		21.9	495	31	-14.9	-16.6	
Foka 008.3	12326.3	mortar		15.0	605	22	-15.79	-17.89	
GETA CHURCH									
Unit: nave (conclu	sive)								
Geka 001-2.1	10599-2.1	moutou	8.0; 46–75	122	162	31	-20.15	22.46	CI CII
OCKa 001-2.1	10377-2.1	mortar	0.0, 40-73	13.3	463	31	-20.13	-22.46	CI, CII
Geka 001-2.1 Geka 001-2.2	10599-2.1	mortar	0.0, 40–73	15.4	455	30	-5.58	-22 <b>.46</b> -18.09	CI, CII
			6.0, 40-73						CI, CII
Geka 001-2.2	10599-2.2	mortar	<b>6.0, 40</b> –73	15.4	455	30	-5.58	-18.09	CI, CII
Geka 001-2.2 Geka 001-2.3	10599-2.2 10599-2.3	mortar mortar	8.0, 40-73	15.4 14.5	455 438	30 28	-5.58 -9.81	-18.09 $-18.7$	ci, cii
Geka 001-2.2 Geka 001-2.3 Geka 001-2.4	10599-2.2 10599-2.3 10599-2.4	mortar mortar mortar	6.0, 40-73	15.4 14.5 14.8	455 438 422	30 28 27	-5.58 -9.81 -12.25	-18.09 -18.7 -18.75	ci, cii
Geka 001-2.2 Geka 001-2.3 Geka 001-2.4 Geka 001-2.5	10599-2.2 10599-2.3 10599-2.4 10599-2.5	mortar mortar mortar mortar	7.0; 46–75	15.4 14.5 14.8	455 438 422 517	30 28 27 31	-5.58 -9.81 -12.25 -12.89	-18.09 -18.7 -18.75	CI, CII
Geka 001-2.2 Geka 001-2.3 Geka 001-2.4 Geka 001-2.5 Geka 001W	10599-2.2 10599-2.3 10599-2.4 10599-2.5 10604	mortar mortar mortar mortar wood	,	15.4 14.5 14.8 41.9	455 438 422 517 426	30 28 27 31 33	-5.58 -9.81 -12.25 -12.89 -23.32	-18.09 -18.7 -18.75 -20.67	ŕ
Geka 001-2.2 Geka 001-2.3 Geka 001-2.4 Geka 001-2.5 Geka 001W <b>Geka 002.1</b>	10599-2.2 10599-2.3 10599-2.4 10599-2.5 10604 <b>10600.1</b>	mortar mortar mortar mortar wood <b>mortar</b>	,	15.4 14.5 14.8 41.9	455 438 422 517 426 <b>444</b>	30 28 27 31 33 <b>31</b>	-5.58 -9.81 -12.25 -12.89 -23.32 <b>-20.25</b>	-18.09 -18.7 -18.75 -20.67	,
Geka 001-2.2 Geka 001-2.3 Geka 001-2.4 Geka 001-2.5 Geka 001W <b>Geka 002.1</b> Geka 002.2	10599-2.2 10599-2.3 10599-2.4 10599-2.5 10604 <b>10600.1</b> 10600.2	mortar mortar mortar mortar wood <b>mortar</b> mortar	,	15.4 14.5 14.8 41.9 <b>18.6</b> 22.0	455 438 422 517 426 <b>444</b> 447	30 28 27 31 33 <b>31</b> 26	-5.58 -9.81 -12.25 -12.89 -23.32 - <b>20.25</b> -4.01	-18.09 -18.7 -18.75 -20.67 -23.74 -18.47	ŕ
Geka 001-2.2 Geka 001-2.3 Geka 001-2.4 Geka 001-2.5 Geka 001W Geka 002.1 Geka 002.2 Geka 002.3	10599-2.2 10599-2.3 10599-2.4 10599-2.5 10604 <b>10600.1</b> 10600.2 10600.3	mortar mortar mortar mortar wood <b>mortar</b> mortar mortar	,	15.4 14.5 14.8 41.9 <b>18.6</b> 22.0 17.7	455 438 422 517 426 <b>444</b> 447 446	30 28 27 31 33 <b>31</b> 26 30	-5.58 -9.81 -12.25 -12.89 -23.32 <b>-20.25</b> -4.01 -10.19	-18.09 -18.7 -18.75 -20.67 - <b>23.74</b> -18.47 -20.07	ŕ

	Lab nr		C yield (%);		14C		$\delta^{13}C$	$\delta^{18}O$		
	Aarhus		grain-size	Fraction	age	$\pm$	<b>‰</b>	<b>‰</b>		
Sample	(AAR-#)	Type	fraction (µm)	size (%)	_	1 σ		VPDB	Criteria	Comments
Geka 002.5	10600.5	mortar		22.8	584	27	-13.03	-20.87		
Geka 003.1	10601.1	mortar	6.5; 46–75	16.3	396	29	-18.44	-21.02	CII	
Geka 003.2	10601.2	mortar	,	17.9	463	27	-5.59	-16.11		
Geka 003.3	10601.3	mortar		16.7	443	31	-11.36	-18.55		
Geka 003.4	10601.4	mortar		16.5	372	36	-12.48	-19.39		
Geka 003.5	10601.5	mortar		32.5	484	28	-13.49	-19.98		
Geka 005.1	10602.1	mortar	7.2; 46–75	17.4	466	37	-20.1	-22.78	CI, CII	
Geka 005.2	10602.2	mortar		19.9	496	30	-2.94	-16.97		
Geka 005.3	10602.3	mortar		17.2	540	28	-9.57	-19.44		
Geka 005.4	10602.4	mortar		18.2	540	26	-11.22	-21.01		
Geka 005.5	10602.5	mortar		27.3	589	32	-12.84	-21.22		
Geka 006C	10605	charcoal			492	28	-24.8			
Dendro: AD 1470–1	475									
HAMMARLAND (										
Unit: early nave (co			5.2 NB	4.5	رم. <del>.</del>	<i>-</i>	10.0	22.1	OI OI	
Haka 018.1	1465.1	mortar	5.3; NR	45	695	65	-12.9	-22.1	CI, CII	
Haka 018.2	1465.2	mortar		55	750	60	-8 26.7	-21.4		
Haka 018 C	1466	charcoal	( 0 20 <b>==</b>	20	820	60	-26.7	20. 1	OI OI	
Haka 042.1	2521.1	mortar	6.9; 39–75	30	725	55	-19.4	-20.4	CI, CII	
Haka 042.2	2521.2	mortar		70	815	50	-11.3	-17.5	CIT	
Haka 052.1	2168.1	mortar	7.2; 63–74	40	690	65	-13.9	-20.3	CII	
Haka 052.2	2168.2	mortar		60	875	70	-8.4	-18.6	CIT	
Haka 052-2.1	2168-2.2.1		2.9; 76–125	19.5	756	44	[-17.04]	[-13.53]	CII	
Haka 052-2.2	2168-2.2.2			17.1	841	43	-3.98	-16.19		
Haka 052-2.3	2168-2.2.3			18.1	882	44	-9.19	-18.52		
Haka 052-2.4	2168-2.2.4			16.9	729	33	-9.72	-19.12		
Haka 052-2.5	2168-2.2.5			28.1	1010	55	-11.04	-19.07		
Haka 52 C	2169	charcoal	60.20.75	20	970	70	-23.1	21.4	CI CII	
Haka 53.1	2522.1	mortar	6.8; 39–75	29	755	45	-16.5	-21.4	CI, CII	
Haka 53.2	2522.2	mortar	5 2. (2.74	71	790	40	-9.6	-19	CI CII	
Haka 54.1	2171.1	mortar	5.2; 63–74	40	710	90	-12	<b>-19.2</b>	CI, CII	
Haka 54.2	2171.2	mortar	E 9. (2.74	60	730	60 50	-10.9	-19.4	CI CII	
Haka 57.1	2174.1	mortar	5.8; 63–74	40	680	50	-12.5	-18.1	CI, CII	
Haka 57.2	2174.2	mortar	5 2 (2 54	60	755 <b>7</b> 05	45	-10.7	-19	CI CII	
Haka 58.1	2176.1	mortar	5.3; 63–74	40	795	50	-11.5	<b>-17.7</b>	CI, CII	
Haka 58.2	2176.2	mortar		60	845	60	-10.4	-19.3		
Haka 58 C Units towar (aanals	2177	charcoal			950	55	-24.1			
U <b>nit: tower <i>(conclu</i> Haka 024W</b>		wood			860	70				
Haka 024W Haka 061 C	<i>Hel-2996</i> 2182	wood			860 1015	70 45	-24.5			
нака 061 С Н <b>ака 062.1</b>	2182 2184.1	charcoal	6.1; 63–74	39	740	70	-24.3 - <b>14.2</b>	-17.8	CI, CII	
Haka 062.1 Haka 062.2	2184.1		0.1, 03-74	<b>6</b> 1	700		-14.2 -11.6	-17.8 -18.1	Ci, Cii	
нака 002.2 Нака 048.1	2080.1	mortar	4.0; 63–74	<b>73</b>	690		-11.6 - <b>12.3</b>	-18.1 - <b>17.6</b>	CII	
Haka 048.1 Haka 048.2	2080.1	mortar	7.0, 03-74	7 <b>3</b> 27	910	45	-12.3 -8.2	-17. <b>0</b> -17	CII	
Haka 048.2 Haka 048 C	2080.2	charcoal		41	745	65	-8.2 -26.2	-1/		
нака 048 С Н <b>ака 049.1</b>	2048 2081.1		8.7; 63–74	31	680	50	-26.2 - <b>13.9</b>	-20.5	CI, CII	
Haka 049.1 Haka 049.2	2081.1	mortar	0.7, 03-74	<b>6</b> 9	660	50 50	-13.9 -9.2	-20.5 -19.5	Ci, Cii	
Unit: vaulting and			onelusiva)	UF	000	50	—y.∠	-17.3		
Haka 009W	Hel-2995	wood	onciusivej		660	75				
Haka 009 W Haka 002 W						70				
	Hel-2994	wood			630 570					
Haka 010W	Hel-3313	wood			570 640	80 80	20.0			
Haka 047W <b>Haka 047.1</b>	2046 <b>2079.1</b>	wood <i>mortar</i>	3.8; 63-74	58	810	50 50	-28.9 - <b>12.4</b>	-19.9	CI	probably
1umu V4/.1	4U/7.1	mortar	5.0, 05-/4	50	010	30	-12.4	-17.7	CI	wrong, old
Haka 047.2	2079.2	mortar		42	800	75	-10.7	-19.1		wood

800 75 -10.7 -19.1

Appendix Dated mortal samples and fractions. (Continued	Appendix	Dated mortal	samples and	fractions.	(Continuea
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Appendix Dated m		anu macti		<i>y</i>	14C		\$13 <i>C</i>	2180		
	Lab nr		C yield (%);	Б .:	<sup>14</sup> C		δ <sup>13</sup> C	$\delta^{18}O$		
	Aarhus		grain-size	Fraction	-	±	<b>‰</b>	<b>‰</b>	a	
Sample	(AAR-#)	Type	fraction (µm)	size (%)	(BP)	1 σ	VPDB	VPDB	Criteria	Comments
Haka 047 C	2047	charcoal			910	75	-24.8			
Haka 045.1	2077.1	mortar	5.7; 63-74	47	815	45	<i>-11.7</i>	-19.4	CI	probably
										wrong, too old
Haka 045.2	2077.2	mortar		53	730	50	-9.2	-19.1	~~~	
Haka 041.1	2072.1	mortar	5.7; 63–74	44	510		-13	-21.9	CII	
Haka 041.2	2072.2	mortar	ND 62 54	56	800	80	-7.6	-19.6	CII	
Haka 055.1	2172.1	mortar	NR; 63–74	39	575		-11.9	-19.4	CII	
Haka 055.2	2172.2	mortar	2.0.76 125	61	845		−10.3 <b>−13.85</b>	-19.5	CI	£1
Haka 055-2.1	2172-2.2.1	mortar	3.0; 76–125	16.8	739	32	-13.63	-18.83	CI	profile youn- ger than result
										from profile in
										2 fractions,
										possibly due to
										different grain-
Halan 055 2.2	2172 2 2 2			17.0	769	20	г ол			size fractions
Haka 055-2.2	2172-2.2.2			17.0	768	30		10.6		
Haka 055-2.3 Haka 055-2.4	2172-2.2.3 2172-2.2.4			16.4 17.1	807 740		-10.25 [-8.68]	-18.6 [-14.32]		
Haka 055-2.5	2172-2.2.4			32.0	825		-10.32	-14.32j -19.28		
Haka 061.1	2172-2.2.3	mortar	6.0; 63–74	43	640		-10.32 - <b>13.3</b>	-19.26 - <b>18.6</b>	CI, CII	
Haka 061.2	2181.2	mortar	0.0, 05-74	<b>5</b> 7	690		-10.4	-18.3	CI, CII	
Haka 044.1	2075.1	mortar	5.3; 63-74	56	615		-12.5	-19.6	CII	
Haka 044.2	2075.2	mortar	0.0, 00	44	760		-10.2	-18.8	011	
Haka 044L.1	2076.1	lime	5.8; not sieved		635		-10.3	-19.3	CI, CII	
Haka 044L.2	2076.2	lime	,	53	660	115	-6.7	-19.9	,	
Haka 046.1	2078.1	mortar	5.6; 63-74	46	625	50	-13.9	-20.9	CII	
Haka 046.2	2078.2	mortar		54	880	55	-8.1	-19.6		
Haka 056.1	2173.1	mortar	6.0; 63–74	37	615	50	-11.9	-18.9	CI, CII	
Haka 056.2	2173.2	mortar		63	675	60	-11	-19.9		
Haka 059.1	2178.1	mortar	7.2; 63–74	33	615		-13	-19	CII	
Haka 059.2	2178.2	mortar		67	730		-11.1	-18.8		
Haka 059C	2179	charcoal		20	1270		-26	40.0	CIT	
Haka 060.1	2180.1	mortar	6.0; 63–74	38	615		-11.9	-19.3	CII	
Haka 060.2	2180.2	mortar	uit aanalusins	62	715	50	-10.5	-19.8		
Unit: "murklack" Haka 001.1	1463.1	_		50	545	65	-10.1	-16.7	CI	
Haka 001.1	1463.1	mortar mortar	4; NK	50	630	70	-10.1 -9.8	-16.7 -16.4	CI	
Haka 001.2	1464	charcoal		30	430		-26.5	-10.4		
Haka 040.1	2071.1	mortar	5.7; 63–74	47	715		-20.3 - <b>12.8</b>	-18.9	CI	
Haka 040.2	2071.2	mortar	3.7, 03 74	53	760		-11.6	-18.6	CI	
Haka 043.1	2074.1	mortar	6.3; 63–74	35	490		-15	-19.8	CII	
Haka 043.2	2074.2	mortar	,	65	690		-14.4	-20.6		
Unit: chancel (con										
Haka 031W	Hel-3260	wood			520	60				
Haka 038.1	2069.1	mortar	7.5; 63–74	36	510	60	-15.2	-21.5	CI, CII	
Haka 038.2	2069.2	mortar		64	600	65	-10.4	-19.8		
Haka 038C	2089	charcoal			570		-25			
Haka 038W	2088	wood			480	50	-25.3			
Haka 039.1	2070.1		7.2; 63–74	43	480		-15.8	-20.9	CIII	
Haka 039.2	2070.2	mortar		57	695	65	-10.7	-17.8		
Unit: chancel roof			,		2.40		16.5	10.2	CIV.	
Haka 051.1	2083.1	mortar	4.6; 63–74	57	340		-16.2	-19.3	CIV	
Haka 051.2	2083.2	mortar		43	730	45	-15.4	-17.6		
Dendro: AD 1466										
Unit: sacristy (con Haka 050.1	,	morton	76.62 74	12	275	E0	14.2	20.7	CIV	
Нака 050.1 Нака 050.2	<b>2082.1</b> 2082.2	mortar mortar	7.6; 63–74	<b>43</b> 57	<b>375</b> 795		<b>−14.3 −11.2</b>	<b>−20.7</b> −18.5	CIV	
Haka 050.2	2082.2	wood		51	450		-25.6	-10.3		
11uKa 050 W	2070	wood			750	00	-23.0			

	Lab nr		C yield (%);		<sup>14</sup> C		δ <sup>13</sup> C	δ <sup>18</sup> O	<u> </u>	
	Aarhus		grain-size	Fraction	age	$\pm$	<b>‰</b>	<b>‰</b>		
Sample	(AAR-#)	Type	fraction (µm)	size (%)	_	1 σ	VPDB	VPDB	Criteria	Comments
HAMNÖ CHAPE	I KÖKAR		va)		. ,					
Hamnkap. 001.1	4236.1	mortar	8.4; 39–75	20	310	35	-18.1	-21.2	CI	
Hamnkap. 001.2	4236.2	mortar	011,00	80	315	45	-12.7	-21	01	
Hamnkap. 002.1	4237.1	mortar	7.7; 39–75	30	460	35	-12.8	-19.7	CI	
Hamnkap. 002.2	4237.2	mortar	. ,	70	440	40	-12.1	-20.2		
Hamnkap. 005.1	4238.1-1	mortar	8.0; 39–75	28	395	40	-16.9	-21.5	CII	
Hamnkap. 005.2	4238.2-1	mortar	,	72	540	65	-13.2	-20.3		
Hamnkap. 005.2.1	4238.2-1	mortar	8.1; 39–75	22	390	45	-18.2	-21.2	CII	
Hamnkap. 005.2.2	4238.2-2	mortar		78	520	50	-13.3	-20.4		
Hamnkap. 006.1	4239.1	mortar	8.9; 39–75	25	365	40	-14.3	-21.2	CII	
Hamnkap. 006.2	4239.2	mortar		75	515	50	-12.7	-22		
JOMALA CHURO										
Unit: nave (conclu	,		7.4.46.75	17.0	0.40	40	11.00	11 12	CI CII	
Joka 030.1	13006.1	mortar	7.4; 46–75	17.0	849	40	-11.08	-11.13	CI, CII	
Joka 030.2 Joka 031.1	13006.2 <b>13144.1</b>	mortar <b>mortar</b>	6.1; 46–75	18.1 <b>12.2</b>	886 <b>817</b>	44 <b>34</b>	-10.55 - <b>11.75</b>	-10.03 - <b>12.01</b>	CI, CII	
			0.1; 40-75						CI, CII	
Joka 031.2 Joka 031.4	13144.2 13144.4	mortar mortar		18.3 14.7	787 885	29 28	-11.81 $-11.72$	-11.3 -11.04		
Joka 031.4 Joka 031.5	13144.4	mortar		17.4	936	29	-11.72 $-11.6$	-11.04 -10.76		
Joka 033W	Oxford	wood		1 / .4	780	15	-11.0	-10.70		
Unit: tower (concl		woou			780	13				
Joka 005.1	4839.1	mortar	8.3; 39–75	27	735	30	-17.7	-22.4	CII	
Joka 005.2	4839.2	mortar	0.5, 57-75	72	865	50	-9.5	-19.5	CII	
Joka 011.1	4836.1	mortar	9.5; 39–75	17	675	25	-19.5	-22.6	CI, CII	
Joka 011.2	4836.2	mortar	7.5, 57 75	83	740	40	-8.3	-19.5	CI, CII	
Joka 013a.1	4835.1	mortar	5.7; 39–75	28	765	30	-22.8	-25	CII	
Joka 013a.2	4835.2	mortar	e, ese	72	900	45	-9.8	-22	011	
Joka 013a.2.1	4835.2.1	mortar	3.6; 39-75	10.3	810	35	-23.35	-22.72	CI, CII	age profile
										within 2 $\sigma$ of result from pro- file in 2 frac- tions
Joka 013a.2.2	4835.2.2	mortar		42.8	865	30	-11.61	-19.42		
Joka 013a.2.3	4835.2.3	mortar		24.1	850	35	-10.01	-19.53		
Joka 013a.2.4	4835.2.4	mortar		22.5	840	30	-11.13	-20.16		
Joka 013a.3.1	4835.3.1	mortar	4.6; 39–75	3.5	825	35	-30.22	-23.97	CII	age profile within $2 \sigma$ of result from profile in 2 fractions
Joka 013a.3.2	4835.3.2	mortar		28.2	907	28	-10.82	-19.48		
Joka 013a.3.3	4835.3.3	mortar		15.0			-12.03	-19.42		
Joka 013a.3.4	4835.3.4	mortar		12.2	890	30	-10.05	-19.17		
Joka 013a.3.5	4835.3.5	mortar		15.0			-10.87	-20.01		
Joka 013a.3.6	4835.3.6	mortar		12.4	886	29	-11.06	-19.89		
Joka 013a.3.7	4835.3.7	mortar		8.0		<b>.</b> -	-11.16	-19.59		
Joka 013a.3.8	4835.3.8	mortar		2.6	1135	50	-11.71	-18.82		
Joka 013a.3.9	4835.3.9	mortar	0.0. 20. 55	3.0	<b>735</b>	20	-11.24	-16.76	CII	
<b>Joka 014.1</b> Joka 014.2	4838.1	mortar	8.9; 39–75	22	735	<b>30</b> 45	<b>−15</b> −8.1	-17.9	CII	
Joka 014.2 Joka 014-2.1	4838.2 4838-2.2.1	mortar	6.3; 46–75	78 <b>17.9</b>	815 <b>879</b>	43 47	-8.1 - <b>14.64</b>	−16.4 <b>−16.29</b>	CI	age profile
Јока 014-2.1	4030-2,2,1	moriar	0.3; 40-/3	17.9	0/9	4/	-14.04	-10.29	CI	older than result from profile in 2 fractions, reason unknown
Joka 014-2.2	4838-2.2.2	mortar		19.2	900	80	-3.1	-12.55		zon ummown
Joka 014-2.3	4838-2.2.3			18.5	893	50	-9.27	-15.04		
0014 01 1 2.3	1030 2.2.3	.11011111		10.5	0,5	20	7.41	15.07		

Appendix Dated mortal samples and fractions. (Continued)
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Appendix Dated mo	ntai sampies	anu maci	ions. (Continued	ı)						
	Lab nr		C yield (%);		<sup>14</sup> C		$\delta^{13}C$	$\delta^{18}O$		
	Aarhus		grain-size	Fraction	age	$\pm$	<b>‰</b>	<b>%</b> o		
Sample	(AAR-#)	Type	fraction (µm)	size (%)	(BP)	1 σ	VPDB	VPDB	Criteria	Comments
Joka 014-2.4	4838-2.2.4	mortar		18.9	930	42	-9.96	-15.36		
Joka 014-2.5	4838-2.2.5	mortar		24.6	1055	47	-10.08	-15.13		
Joka 016.1	4837.1	mortar	8.8; 39–75	20	715	30	-20.9	-21.5	CII	
Joka 016.2	4837.2	mortar	,	80	925	40	-10.9	-18.2		
Dendro: AD 1283										
KUMLINGE CHU	JRCH									
Unit: nave, west ga	,	,								
Kumka 001.1	11852.1	mortar	2.8; 46–75	17.4	428	34	-15.07	-17.23	CI	
Kumka 001.2	11852.2	mortar		18.8	495	27	-4.21	-13.21		
Kumka 001.3	11852.3	mortar	- 4 46	25.0	528	28	-9.4	-16.1	OT OT	
Kumka 002.1	11853.1	mortar	7.4; 46–75	18.5	535	29	-15.18	-18.1	CI, CII	
Kumka 002.2	11853.2	mortar		24.9	516	29	-6.64	-17.31		
Kumka 002.3	11853.3	mortar	7.4.46.75	25.1	489	26	-10.78	-17.31	CI CII	
Kumka 003.1	12319.1	mortar	7.4; 46–75	18.5	512	36	-16.88	-15.77	CI, CII	
Kumka 003.2 Kumka 003.3	12319.2 12319.3	mortar mortar		24.9 25.1	491 583	42 40	-5.56 -9.59	-11.99 -13.6		
Unit: nave east gal				23.1	363	40	-9.39	-13.0		
Kumka 004.1	11854.1	mortar	7.5; 46–75	14.6	250	27	-11.36	-15.98		
Kumka 004.2	11854.2	mortar	7.5, 10 75	23.6	632	49	-8.24	-15.19	nlateau	fire damage
Kumka 004.3	11854.3	mortar		24.3	607	34	-11.72	-18.05	praceau	me damage
Kumka 004.4	11854.4	mortar		24.1	603	31	-11.93	-18.3		
Kumka 004.5	11854.5	mortar		13.4	806	27	-12.29	-18.15		
Kumka 005.1	12320.1	mortar	6.0; 46–75	10.8	294	48	-15.54	-18.19		
Kumka 005.2	12320.2	mortar	ŕ	23.8	420	34	-4.87	-16.02		
Kumka 005.3	12320.3	mortar		23.7	550	35	-9.21	-17.89	plateau	fire damage
Kumka 005.4	12320.4	mortar		21.2	549	25	-10.63	-19.32		
Kumka 005.5	12320.5	mortar		20.4	678	25	-11.29	-18.98		
Kumka 006.1	12321.1	mortar	5.6; 46–75	9.0	107	33	-16.18	-17.22		
Kumka 006.2	12321.2	mortar		21.2	401	34	-8.11	-15.65	plateau	probably later
Kumka 006.3	12321.3	· · · · · · · · · · · · · · · · · · ·		20.7	420	34	-10.86	-15.61		repair
Kumka 000.3 Kumka 006.4	12321.3	mortar mortar		21.5	464	27	-10.60 $-11.62$	-13.61 -18.61		
Kumka 006.5	12321.5	mortar		27.5	616	29	-11.62 -11.69	-18.82		
Unit: tower stairca				27.5	010	2)	11.07	10.02		
Kumka 007.1	13005.1	mortar	5.7; 46–75	9.9	440	39	-15.63	-19.36	CIV	too few sam- ples analyzed
Kumka 007.2	13005.2	mortar		22.7	573	26	-6.1	-16.11		pres unary zea
Kumka 007.3	13005.3	mortar		18.9	543	36	-10.16	-18.44		
KÖKAR CHURC										
Unit: chancel (inco	,									
Kökar 010.1	13147.1	mortar	8.6; 46–75	9.3	775	48	-16.13	–11.91	test sample	atypical pro- file, test using
Kökar 010.2	13147.2	mortar		11.4	751	31	-15.64	-10.88		HCl hydrolysis
Kökar 010.2 Kökar 010.3	13147.2	mortar		11.4	734	34	-15.04 -16.22	-10.88		
Kökar 010.4	13147.4	mortar		16.8	634	30	-15.65	-9.96		
Kökar 010.5	13147.5	mortar		50.4	637	34	-15.04	-11.09		
							- • • •			
LEMBÖTE CHAI	PEL									
Unit: east gable (co										
Lembo 3.1	4232.1		5.4; 39–62	41	590	30	-15.9	-18.2	CII	
Lembo 3.2	4232.2	mortar		59	775	55	-17.3	-19.7		
Lembo 4.1	4233.1	mortar	4.4; 39–62	50	675	35	-19.4	-20.8	CII	
Lembo 4.2	4233.2	mortar	5 C 20 C2	50	785	50	-20.2	-23.1	CII	
Lembo 5.1	4234.1	mortar	5.6; 39–62	32	610	40	-16.9	-19.7	CII	
Lembo 5.2	4234.2	mortar		68	755	55	-18.5	-21		

	Lab nr		C yield (%);		<sup>14</sup> C		$\delta^{13}C$	$\delta^{18}O$		
	Aarhus		grain-size	Fraction	age	±	‰	<b>‰</b>		
Sample	(AAR-#)	Type	fraction (µm)	size (%)	(BP)	1 σ	VPDB	VPDB	Criteria	Comments
Lembo 8.1	4235.1	mortar	5.6; 39–62	32	705	45	-12.8	-20.6	CI, CII	
Lembo 8.2	4235.2	mortar	,	68	770		-10.9	-22	- , -	
Lembo-1.1	3186.1	mortar	8.5; 39–62	65	710	35	-18.9	-19.4	CII	
Lembo-1.2	3186.2	mortar		35	815		-19	-20.3		
Lembo-2.1	3187.1	mortar	5.8; 39–62	34	580		-12	<b>-18.8</b>	CII	
Lembo-2.2	3187.2	mortar		66	795	35	[-12]			
LEMLAND CHU	JRCH									
Unit: nave (concl	usive)									
Leka 021.1	13145.1	mortar	2.3; 46–75	34.2	821	31	-6.29	<b>-4.97</b>	CI	
Leka 021.2	13145.2	mortar		26.5	836	29	-6.81	-4.72		
Leka 021.3	13145.3	mortar		27.7	875	29	-7.12	-5.09		
Dendro: AD 1239										
Dendro: AD 1285										
Dendro: AD 1292 Unit: tower (cond										
Leka 002.1	4808.1	mortar	5.4; 39–75	28	595	30	-10.3	-13	CIII	
Leka 002.2	4808.2	mortar	3.1,07 78	72	760	45		-14.6	CIII	
Leka 003c	4809	charcoal		, <b>-</b>	725		-22.5	1		
Leka 004c	4810	charcoal			710		-21.7			
Leka 006c	4811	charcoal			945	20	-23.8			
Leka 007.1	4812.1	mortar	4.4; 39–75	32	475	30	-10.1	-18		alkaline sample
Leka 007.2	4812.2	mortar		68	715	40	-8.5	-18.1		_
Leka 008.1	4814.1	mortar	5.8; <39	26	710		-18.2	-20.4	CI	
Leka 008.2	4814.2	mortar		74	650	40		-17.7		
Leka 008c	4813	charcoal			870		-24.3			
Leka 009.1	4815.1	mortar	7.5; 39–75	21	665		-18.5	-20.9	CIII	
Leka 009.2 Dendro: AD 1318	4815.2	mortar		79	785	40	-9.4	-24		
Deligio. AD 1516										
SALTVIK CHUI										
Unit: sacristy and	,		,	••					OT OH	
Saka 119.1	2534.1	mortar	7.8; 63–74	29	655	60		-11	CI, CII	
Saka 119.2	2534.2	mortar	(0. (2.74	71	780	110	-3	-9.8	CI CII	
Saka 120.1	2535.1	mortar	6.9; 63–74	33	[760]	45 90	[-15]	14.2	CI, CII	
Saka 120.2 Saka 121.1	2535.2 <b>2536.1</b>	mortar <b>mortar</b>	6.8; 63–74	77 <b>34</b>	740 <b>665</b>		−7.6 <b>−11.6</b>	−14.2 <b>−17.3</b>	CII	
Saka 121.1 Saka 121.2	2536.2	mortar	0.0, 05-74	66	770	55		-17.3 $-16.2$	CII	
Saka 121-2.1	2536-2.2.1		5.0; 76–125	20.0	448		-10.8	-10.2		profile youn-
Suku 121 2.1	2330 2.2.1	mortur	3.0, 70 123	20.0	770	73	10.0	10.0		ger than result
										from profile in
										2 fractions,
										possibly due to different grain-
										size fractions
Saka 121-2.2	2536-2.2.2			14.4	559	49	-5.89	-5.89		
Saka 121-2.3	2536-2.2.3			14.6	580	55	-9.26	-9.26		
Saka 121-2.4	2536-2.2.4			13.7	499	44	-9.04	-9.04		
Saka 121-2.5	2536-2.2.5		70 (2 T)	37.3	642	38		-9.44	OI OI	
Saka 122.1	2537.1	mortar	7.9; 63–74	<b>30</b>	750		-16.7	-19.6	CI, CII	
Saka 122.2 Saka 122-2.1	2537.2 2537.2 1	mortar	69.76 125	70 13 3	865		-11.7	-17.5	CI CII	
Saka 122-2.1 Saka 122-2.2	<b>2537-2.1</b> 2537-2.2	mortar mortar	6.8; 76–125	<b>13.3</b> 16.2	<b>763</b> 751		<b>−16.55 −10.02</b>	<b>−17.45</b> −15.95	CI, CII	
Saka 122-2.2 Saka 122-2.3	2537-2.2	mortar		15.9	825		-10.02 -12.98	-13.93 -17.48		
Saka 122-2.3	2537-2.3	mortar		18.5	740		-12.36 $-13.36$	-17.46 $-17.26$		
Saka 122-2.5	2537-2.5	mortar		36.5	840		-13.53	-17.20 $-16.52$		
Saka 132.1	3013.1	mortar	7.0; 39–62	39	720		<b>-7.3</b>	-13.8	CI, CII	

Appendix Dated mortal samples and fractions. (Continued	Appendix	Dated mortal	samples and	fractions.	(Continued
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Appendix Dated mo	ortai sampies	and Iraci	•	<i>a)</i>						
	Lab nr		C yield (%);		<sup>14</sup> C		$\delta^{13}C$	$\delta^{18}O$		
	Aarhus		grain-size	Fraction	age	$\pm$	<b>‰</b>	<b>‰</b>		
Sample	(AAR-#)	Type	fraction (µm)	size (%)	(BP)	1 σ	VPDB	VPDB	Criteria	Comments
Saka 132.2	3013.2	morter		61	790	35	-7.7	-13.9		
		mortar	5 9. 63 74						CI CII	
Saka 147.1	4563.1	mortar	5.8; 63–74	34	<b>705</b> 695	<b>35</b> 50	<b>-9.8</b> -9.6	<b>-14.9</b>	CI, CII	
Saka 147.2	4563.2	mortar		66	093	30	-9.0	-14.8		
Unit: rebuilding of		· .			520	70				
Saka 107W	Hel-3561	wood			520	70				
Saka 108W	Hel-3562	wood	( 9, (2, 74	20	640	70	22.4	22.0	CII	
Saka 103.1	2524.1	mortar	6.8; 63–74	29	595	45	-22.4	-22.9	CII	
Saka 103.2	2524.2	mortar	77. (2.74	71	865	60	-10.6	-18.4	CII	
Saka 104.1	2525.1	mortar	7.7; 63–74	29	625	45	-12.1	-17	CII	
Saka 104.2	2525.2	mortar	77. (2)	71 25	1385	50	-6.8	-14.6	CL CH	
Saka 105.1	2995.1	mortar	7.7; <62	35	645	30	-11.7	-16.3	CI, CII	
Saka 105.2	2995.2	mortar	0.1(2	65	690	25	-10.4	-16	CII	
Saka 106.1	2996.1	mortar	8.1; <62	43	625	30	<b>-7.8</b>	-11.9	CII	
Saka 106.2	2996.2	mortar	<b>5</b> .0 -63	57 <b>5</b> 0	700	40	-9.2	-12.8	CII	
Saka 109.1	2997.1	mortar	7.8; <62	50	625	30	-8.6	-14.1	CII	
Saka 109.2	2997.2	mortar	C = 20 C2	50	705	30	<del>-9</del> .4	-14.9	CIT	
Saka 133.1	3014.1	mortar	6.5; 39–62	43	635	40	-10	-16	CII	
Saka 133.2	3014.2	mortar	<b>T</b> 0 20 62	57	765	35	-10.5	-16.5	CIT	
Saka 146.1	4562.1	mortar	7.0; 39–62	27	615	40	-9.6	-15.5	CII	
Saka 146.2	4562.2	mortar		73	900	55	-8.4	-15.9		
Saka 146-2.1	4562-2.1	mortar	6.1; 63–74	16.5	632	44	-9.69	-14.36	CII	
Saka 146-2.2	4562-2.2	mortar		19.0	810	65	-7.46	-13.38		
Saka 146-2.3	4562-2.3	mortar		18.7	895	55	-9.15	-15.08		
Saka 146-2.4	4562-2.4	mortar		20.8	894	46	-9.46	-15.09		
Saka 146-2.5	4562-2.5	mortar		24.2	948	48	-9.2	-14.71		
Saka 148.1	4241.1	mortar	7.2; 39–75	34	645	35	-9.6	-13.8	CII	
Saka 148.2	4241.2	mortar		66	735	35	-8.9	-14		
Saka 148-2.1	4241-2.1	mortar	6.6; 39–62	17.3	613	43	-11.87	-14.05	CI, CII	
Saka 148-2.2	4241-2.2	mortar		18.1	615	48	-6.13	-6.13		
Saka 148-2.3	4241-2.3	mortar		18.2	730	60	<del>-9</del>	-13.14		
Saka 148-2.4	4241-2.4	mortar		18.5	665	55	-9.41	-12.52		
Saka 148-2.5	4241-2.5	mortar		28.2	758	41	-9.86	-14.04		
Saka 151.1	4564.1	mortar	7.1; 39–75	28	600	45	-10.3	-14.8	CII	
Saka 151.2	4564.2	mortar		72	705	50	-9.1	-15.3		
Saka 152.1	4242.1	mortar	7.6; NR	29	610	40	-10.6	-13.6	CI, CII	
Saka 152.2	4242.2	mortar		71	645	45	-8.5	-14.8		
Dendro: AD 1373										
Unit: tower (concl.	usive)									
Saka 163W	5421	wood			615	35	-26.4			
Saka 164W	5422	wood			670	30	-23.1			
Saka 165W	5423	wood			650	30	-23			
Saka 110.1	2998.1	mortar	6.3; <62	44	620	35	-10.6	-19.7	CII	
Saka 110.2	2998.2	mortar	•	56	790	40	-9.5	-20.1		
Saka 113.1	2529.1	mortar	8.2; 63-74	32	670	45	-15.3	-19.5	CII	
Saka 113.2	2529.2	mortar	*	68	840	50	-7	-16.4		
Saka 153W	4243	wood			690	45	-24			
Saka 118.1	2533.1	mortar	6.9; 63-74	35	630	55	-13.3	-20.5	CII	
Saka 118.2	2533.2	mortar	,	65	815	60	<b>-9.7</b>	-19.2	- *	
Saka 155.1	4246.1	mortar	6.2; 39–62	35	670	35	-22.3	-20.9	CI, CII	
Saka 155.2	4246.2	mortar	. ,	65	675	35	-20.5	-21	- ,	
Dendro: AD 1381								•		
Unit: tower upper	level (concl	usive)								
Saka 115W	Hel-3565	wood			495	45				
Saka 114.1	2530.1	mortar	7.8; 63–74	31	495	45	-15.8	-20	CII	
Saka 114.1 Saka 114.2	2530.1	mortar	, 00 17	69	590	55	-7.8	-17.6	C11	
Saka 114.2 Saka 116.1	3000.1	mortar	6.2; <62	35	535	30	-7.8 - <b>16.7</b>	-20.4	CII	
Saka 116.1 Saka 116.2	3000.1	mortar	····	65	630	35	-10.7 -12.3	-19.1	<b></b>	
Saka 117.1	3000.2		6.4; <62	<b>36</b>	<b>590</b>		-12.3 - <b>15.1</b>	-19.1 - <b>19</b>	CII	
~****** ***/**	2001.1	mor tar	J , J.	-0	270	00	10.1	-/	~	

	Appendix	Dated mortal	samples and	fractions.	(Continued
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	T =1= ····		C ====1.1 (0/)		140		\$13 <i>C</i>	2180		
	Lab nr		C yield (%);	F	14C		δ <sup>13</sup> C	δ <sup>18</sup> O		
Sampla	Aarhus	Type	grain-size	Fraction		±	‰ VPDB	‰ VPDB	Criteria	Comments
Sample	(AAR-#)	Type	fraction (µm)	size (%)		1 σ			Criteria	Comments
Saka 117.2	3001.2	mortar	# # OC 12	64	780	30	-11.5	-17.6		
Saka 125.1	3006.1	mortar	7.7; 39–62	34	715	35	-11.1	-19.2		
Saka 125.2	3006.2	mortar		66	830	35	-6.5	-18.1	~~~	
Saka 126b.1	3007.1	mortar	6.6; 39–62	36	585	50	-13	-22.5	CII	
Saka 126b.2	3007.2	mortar		64	710	30	-8.8	-22	~~~	
Saka 154-2.1	4244.1	mortar	7.6; NR		480	35	-10.6	-13.6	CII	
Saka 154-2.2	4244.2	mortar			625	40	-8.2	-14.8		
Saka 154W	4245	wood			580	40	-23.6			
Unit: nave west ga	Hel-3332				540	90				
Saka 013W Saka 111W	Hel-3563	wood wood			530	80 70				
Saka 111W Saka 112W	Hel-3564	wood			480	75				
Saka 112 W Saka 129a.1	3009.1	mortar	7.1; 39–62	31	490 490	40	-21.3	-20.9	CII	
Saka 129a.2	3009.2	mortar	7.1, 37-02	69	655	30	- <b>21.3</b> -19	-20.4	CII	
Saka 129b.1	3010.1	mortar	6.7; 39–62	30	460	30	-18.1	-18.9	CII	
Saka 129b.2	3010.2	mortar	0.7, 57 02	70	600	35	-16.9	-18.2	CII	
Saka 130.1	3011.1	mortar	7.1; 39–62	30	475	30	-18.3	-19.9	CII	
Saka 130.2	3011.2	mortar	, 0> 0=	70	605	35	-17.3	-19.4	011	
~				, -			- / 10			
SUND CHURCH										
Unit: nave (fire da	ımage, conc	lusive?)								
Suka 014.1	7563.1	mortar	5.9; 46-75	14.4	496	32	-22.26	-21.96		
Suka 014.2	7563.2	mortar		15.7	683	33	-11.69	-19.74		
Suka 014.3	7563.3	mortar		23.3	781	33	-10.81	-17.76	plateau	
Suka 014.4	7563.4	mortar		18.8	777	36	-13.09	-19.78		
Suka 014.5	7563.5	mortar		27.8	819	33	-13.87	-19.47		
Suka 017.1	7564.1	mortar	5.9; 46–75	15.2	619	42	-24.69	-22.49		
Suka 017.2	7564.2	mortar		16.6	723	49	-15.13	-18.43		
Suka 017.3	7564.3	mortar		18.1	745	60	-18.84	-20.22	plateau	
Suka 017.4	7564.4	mortar		19.1	745	65	-20.22	-20.94		
Suka 017.5	7564.5	mortar	60.46.75	31.1	[775]	65	-22.47	-20.64		
Suka 024.2.1	7567.2.1	mortar	6.9; 46–75	14.6	503	38	-18.01	-18.41		
Suka 024.2.2 Suka 024.2.3	7567.2.2 7567.2.3	mortar mortar		19.8 21.9	675 735	35 38	-11.74 -13.6	-17.81 -19.87	plateau	
Suka 024.2.4	7567.2.4	mortar		20.4	669	28	-13.0 -14.01	-19.57 -19.57	piateau	
Suka 024.2.5	7567.2.5	mortar		23.4	805	37	-14.25	-19.17		
Suka 025.1	7568.1	mortar	4.2; 46–75	17.1	242	47	-14.23 -19.93	-17.17		
Suka 025.2	7568.2	mortar	, , , ,	22.4	450	50	-8.4	-16.42		
Suka 025.3	7568.3	mortar		19.5	742	41	-10.63	-19.03	plateau	
Suka 025.4	7568.4	mortar		14.2	790	50	-11.81	-18.19		
Suka 025.5	7568.5	mortar		26.7	[545]		-12.96	-19.98		
Suka 026-2.1	7569-2.1	mortar	5.3; 46-75	18.0	315	29	-16.01	-17.97		
Suka 026-2.2	7569-2.2	mortar		20.1	732	33	-7.26	-16.2	plateau	
Suka 026-2.3	7569-2.3	mortar		20.6	<b>790</b>	30	-9.74	-17.79		
Suka 026-2.4	7569-2.4	mortar		21.3	546	36	-11.4	-18.18		
Suka 026-2.5	7569-2.5	mortar		20.0	541	36	-12.25	-17.47		
Suka 002.1	7559.1	mortar	4.0; 46–75	16.0	936	36	-24.95	-22.66	incon-	Results too
									clusive	old? Sample
										from founda- tion level
Suka 002.2	7559.2	mortar		13.6	938	38	-18.66	-20.1		tion icvei
Suka 002.2 Suka 002.3	7559.3	mortar		70.4	916	35	-22.3	-20.1 $-23.51$		
Suka 002.2.1	7559.2.1	mortar	3.2; 46–75	15.4	992	34	-24.55	-22.71	incon-	Results too
Sum 002.2.1	1009.4.1	mortui	5.2, 40-75	13.7	114	57	27.33	22./1	clusive	old? Sample
										from founda-
										tion level
Suka 002.2.2	7559.2.2	mortar		23.8	905	36	-20.22	-21.65		
Suka 002.2.3	7559.2.3	mortar		24.3	952	37	-22.13	-22.68		

Appendix Dated mortal samples and fractions. (Continued)

	Lab nr		C yield (%);		<sup>14</sup> C		$\delta^{13}$ C	$\delta^{18}O$		
	Aarhus		grain-size	Fraction	_	±	<b>‰</b>	<b>‰</b>		
Sample	(AAR-#)	Type	fraction (µm)	size (%)	(BP)	1 σ	VPDB	VPDB	Criteria	Comments
Suka 002.2.4	7559.2.4	mortar		21.9	988	36	-22.43	-22.86		
Suka 002.2.5	7559.2.5	mortar		10.8	979	37	-22.42	-22.68		
Suka 002C	7598	charcoal			1555	38	-25.07			
Suka 028.1	8721.1	mortar	3.0; 46–75	24.6	246	43	[-12]	-15.84	incon- clusive	atypical age profile
Suka 028.2	8721.2	mortar		26.2	697	34		-17.12		•
Suka 028.3	8721.3	mortar		24.2	1182	38		-18.77		
Suka 028.4	8721.4	mortar		23.4	768	41	-10.79			
Suka 028.5	8721.5	mortar		1.7	lost					
Suka 028Li.1	8722-2.1	mortar	9.6, 76–150	57.8	192	35	-10.61	-20.01	CI	probably dates documented re pairs after fire
Suka 028Li.2	8722-2.2	mortar		28.3	219	40	-10.34	-19.95		P
Suka 028Li.3	8722-2.3	mortar		14.1	253		-9.28	-19.61		
Suka 028Li.5	8722-2.5	mortar		65.9	279	40	-10.26	-21.26		
Unit: west gable	of nave (fire		nconclusive)							
Suka 019.1	7565.1	mortar	8.9; 46–75	0.26	497	36	-12.38	-17.98		age profile in- sufficient
Suka 019.2	7565.2	mortar		0.36	602	36	-9.15	-17.97		
Suka 019.3	7565.3	mortar		0.38	660	31	-11.42	-18.72		
Suka 020.1	7566.1	mortar	8.7; 46–75	0.24	695	36	-15.29	-18.47		atypical age profile
Suka 020.2	7566.2	mortar		0.34	625	35	-10.92	-18.15		•
Suka 020.3	7566.3	mortar		0.41	610	37	-12.86	-19.05		
Unit: tower (fire	damage, con	clusive)								
Suka 001W	1475	wood			510		-24.8			
Suka 005W	7599	wood			623	38	-23.62			
Suka 007W	7600	wood			659	38	-24.61			
Suka 006.1	7560.1	mortar	6.2; 46–75	10.2	435		-16.34	-15.38		
Suka 006.2	7560.2	mortar		14.3	509	40		-12.61	plateau	
Suka 006.3	7560.3	mortar		13.4	679	33		-12.21		
Suka 006.4	7560.4	mortar		13.9	706		-10.58	-14.37		
Suka 006.5	7560.5	mortar		48.3	499		-11.2	-14.21		
Suka 027.1	8720.1	mortar	3.4; 46–75	27.6	325		-15.4	-17.83	incon- clusive	atypical age profile
Suka 027.2	8720.2	mortar		22.5	1024	41	-8.4	-17.16		
Suka 027.3	8720.3	mortar		20.3	924		-10.7	-18.52		
Suka 027.4	8720.4	mortar		19.6	594		-11.97	-18.83		
Suka 027.5	8720.5	mortar		9.3	990		-12.29	-18.27		
Suka 038.1	7572.1	mortar	5.4; 46–75	17.5	580		-13.31	-16.88		
Suka 038.2	7572.2	mortar		21.7	690		<b>-7.81</b>	-14.64		
Suka 038.3	7572.3	mortar		18.0	668		-11.05	-17.44	plateau	
Suka 038.4	7572.4	mortar		16.9	664		-11.37	-16.08		
Suka 038.5	7572.5	mortar		26.0	744		-10.93	-16.76		
Suka 035.1	7571.1	mortar	6.2; 46–75	25.4	572		-14.45	-19.14	incon- clusive	uncertain inter- pretation
Suka 035.2	7571.2	mortar		37.9	776		-8.14	-17.04		of age profile
Suka 035.3	7571.3	mortar	77.46.75	36.7	857		-10.71	-17.58		
Suka 040.1	7573.1	mortar	7.7; 46–75	25.4	630	37	-14.38	-15.32	incon- clusive	uncertain inter- pretation of age profile
Suka 040.2	7573.2	mortar		39.5	904	36	-8.92	-13.19		r
Suka 040.3	7573.3	mortar		35.0	1147		-10.73	-13.83		
Suka 044.1	7574.1	mortar	6.2; 46–75	24.6	290		-15.72	-15.11	incon- clusive	uncertain inter- pretation of age profile
Suka 044.2	7574.2	mortar		35.7	605	39	-7.3	-15.27		r
Suka 044.3	7574.3	mortar		39.7	585	31	-9.85	-14.59		
Sana O I T.J	1517.5	morum		27.1	202	51	7.00	1 1.57		

	Lab nr		C yield (%);		14C		$\delta^{13}C$	$\delta^{18}O$		
	Aarhus		grain-size	Fraction	age	±	<b>‰</b>	<b>‰</b>		
Sample	(AAR-#)	Type	fraction (µm)	size (%)	(BP)	1 σ	VPDB	VPDB	Criteria	Comments
Unit: sacristy, b	urial chambe	r (conclus	ive)							
Suka 010.1	7561.1	mortar	3.0; 46–75	21.3	354	36	-20.03	-23.3	CI	
Suka 010.2	7561.2	mortar		25.0	420	55	-13.07	-15.69		
Suka 010.3	7561.3	mortar		27.3	318	39	-16.04	-19.11		
Suka 010.4	7561.4	mortar		22.6	385	37	-16.17	-17.83		
Suka 010.5	7561.5	mortar		3.8	548	45	[-17]			
Unit: sacristy <i>(ii</i>	nconclusive)									
Suka 013.2.1	7562.2.1	mortar	6.1; 46–75	16.0	189	34	-13.28	-15.28	incon- clusive	secondary re- pair in sacristy?
Suka 013.2.2	7562.2.2	mortar		19.6	399	39	-10.64	-14.6		
Suka 013.2.3	7562.2.3	mortar		17.6	459	36	-11.93	-15.84		
Suka 013.2.4	7562.2.4	mortar		17.1	492	31	-12.17	-16.64		
Suka 013.2.5	7562.2.5	mortar		29.7	603	37	-12.05	-17.12		
Suka 015.1	9058.1	mortar	3.9; 46–75	18.1	627	37	-19.3	-20.6	incon- clusive	uncertain inter- pretation of age profile
Suka 015.2	9058.2	mortar		17.2	794	38	-9.89	-15.29		
Suka 015.3	9058.3	mortar		17.4	888	37	-13.09	-16.06		
Suka 015.4	9058.4	mortar		17.1	886	29	-15.25	-18.86		
Suka 015.5	9058.5	mortar		30.8	987	46	-15.74	-18.72		
Suka 016.1	9059.1	mortar	3.7; 46–75	19	463	36	-12.76	-13.02	incon- clusive	uncertain inter- pretation of age profile
Suka 016.2	9059.2	mortar		21.6	579	37	-7.88	-10.94		_
Suka 016.3	9059.3	mortar		22.4	568	43	-11.56	-12.7		
Suka 016.4	9059.4	mortar		21.6	703	34	-12.77	-12.88		
Suka 016.5	9059.5	mortar		16.1	778	35	[-13]			
Suka 016C	9057	charcoal			681	38	-24.98			
Suka 034.1	7570.1	mortar	4.6; 46–75	16.9	451	43	-13.5	-18.11	incon- clusive	uncertain inter- pretation of age profile
Suka 034.2	7570.2	mortar		27.7	743	39	-8.06	-15.49		•
Suka 034.3	7570.3	mortar		23.1	728	39	-10.11	-17.36		
Suka 034.4	7570.4	mortar		20.6	835	33	-10.74	-16.25		
Suka 034.5	7570.5	mortar		11.7	1275	38	-10.78	-16.14		
VÅRDÖ CHUR										
Unit: nave, east Vaka 001.1	gable (conclu 8947.1	<b>sive)</b> mortar	10.76.150	18.5	287	36	-21.01	-21.56	incon-	haarii aantami
vики 001.1	0947.1	mortar	4.9; 76–150	10.5	207	30	-21.01	-21.50	clusive	heavy contami- nation
Vaka 001.2	8947.2	mortar		17.1	857	40	-4.79	-16.16		
Vaka 001.3	8947.3	mortar		19.4	933	50	-11.06	-19		
Vaka 001.4	8947.4	mortar		17.1	905	55	-11.78	-19.36		
Vaka 001.3.1	8947.3.1	mortar	5.2; 46-75	9.5			-16.22	-20.64		
Vaka 001.3.2	8947.3.2	mortar	,	17.8	503	37	-12.61	-20.14		
Vaka 002.1	8948.1	mortar	5.0; 76–150	18.9	319	43		[-29.52]	incon- clusive	heavy contami- nation
Vaka 002.2	8948.2	mortar		18.2	979	45	[-2.35]	[-15.98]		
Vaka 002.3	8948.3	mortar		18.2	1274	47	-9.12	-18.65		
Vaka 002.4	8948.4	mortar		17.9	1258	42	-10.09	-19.15		
Vaka 002.5	8948.5	mortar		27.2	1167	44	-11.25	-19.26		
Vaka 002.3.1	8948.3.1	mortar	5.1; 46–75	10.3	524	31	-16.72	-20.86		
Vaka 002.3.2	8948.3.2	mortar		22.6	686	43	-11.04	-19.86		
Vaka 003.1	8949.1	mortar	3.8; 76–150	18.0	240	90	-16.36	-19.91	incon- clusive	heavy contami- nation
Vaka 003.2	8949.2	mortar		21.4	1611	32	-2.88	-14.14		
Vaka 003.3	8949.3	mortar		17.0	2181	36	-6.71	-15.6		
Vaka 003 4	9040-4	mortor		16.5	1596	26	8.02	16.8		

16.5 1586 36 -8.02 -16.8

8949.4

mortar

Vaka 003.4

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Appendix Dated mortal samples and fractions. (Continued)

	Lab nr		C yield (%);		<sup>14</sup> C		$\delta^{13}C$	$\delta^{18}O$		
	Aarhus		grain-size	Fraction	age	±	<b>‰</b>	<b>‰</b>		
Sample	(AAR-#)	Type	fraction (µm)	size (%)	(BP)	1 σ	VPDB	VPDB	Criteria	Comments
Vaka 003.5	8949.5	mortar		27.5	1495	55	-9.58	-17.13		_
Vaka 005C	9056	charcoal			394	41	-26.04			
Vaka 005.1	13006.1	mortar	4.0; 46–75	11.5	415	37	-20.34	-22.5	CIV	agrees with em-
										bedded char- coal (Vaka 005C)
Vaka 005.2	13006.2	mortar		14.7	702	32	-9.24	-18.44		,
Vaka 005.3	13006.3	mortar		13.3	1156	28	-7.78	-17.17		
Vaka 005.4	13006.4	mortar		27.7	1951	34		-17.4		
Dendro: AD 1470-	-75									