Kilowatt-level supercontinuum generation in a single-stage random fiber laser with a half-open cavity

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Abstract The random distributed-feedback fiber laser (RFL) is a new approach to obtain a high-power stable supercontinuum (SC) source. To consider both structure simplification and high-power SC output, an innovative structure achieving a kilowatt-level SC output in a single-stage RFL with a half-open cavity is demonstrated in this paper. It consists of a fiber oscillator, a piece of long passive fiber, and a broadband coupler, among which the broadband coupler acting as a feedback device is crucial in SC generation. When the system has no feedback, the backward output power is up to 298 W under the pump power of 1185 W. When the feedback is introduced before the pump laser, the backward power loss can be reduced and the pump can be fully utilized, which could promote forward output power and conversion efficiency significantly. Under the maximum pump power of 1847 W, a 1300 W...
SC with spectrum ranging from 887 to 1920 nm and SC conversion efficiency of 66% is obtained. To the best of our knowledge, it is the simplest structure used for high-power SC generation, and both the generated SC output power and the conversion efficiency are highest in the scheme of half-opened RFL output SC.

Key words: high-power supercontinuum; random fiber laser; single-stage structure; high conversion efficiency

I. INTRODUCTION

Supercontinuum (SC) with rich spectral compositions and laser properties experienced rapid growth since the photonic crystal fiber (PCF) was born in 1996 [1]. As an research hotpot of SC, the high-power SC has received great attention due to their applications in hyperspectral lidar, optoelectronic countermeasure, and astronomical optical frequency combs [2, 3]. As a nonlinear medium used for SC generation, the PCF with a small core size is not conducive to the scaling of SC output power [4], the large mode area (LMA) fiber is an appropriate choice. At present, the major scheme used for high-power SC generation based on the LMA fiber is to employ the main oscillation power amplifier structure [5, 6]. However, this scheme has not only the complex structure, but also the risk of laser damage due to improper operations, such as the self-excited oscillation caused by the amplified spontaneous emission.

SC generation in a single-stage structure can not only lower the cost and the packaging difficulty, but also reduce the security risks. In 2022, a 791 W SC ranging from 1000 nm to 1500 nm was realized in a quasi-continuous wave fiber oscillator. However, the spectral performance is
not ideal even in the high peak pump of 34 kW [7]. Compared with this scheme, the random distributed-feedback fiber laser (RFL) consisting of a continuous wave (CW) fiber oscillator has a simpler structure with the unique features, such as low background noise, sound robustness, and is free of the photon darkening effect [8]. The output power of the near single-mode fiber oscillator had reached 8 kW in 2020 [9], which lays the foundation for the realization of the single-stage high-power RFL. Based on a fiber oscillator, the single-wavelength kilowatt-level RFLs with a half-open cavity and a full-open cavity have been reported [10, 11]. In 2022, a kilowatt RFL with a full-open cavity was demonstrated experimentally [11]. A short passive fiber length is crucial in this point-reflector-free RFL to enable a one direction output due to the reduced accumulation of backward Rayleigh scattering light, only setting to 35 m in the experiment. However, in the SC generation, a long fiber is required to obtain sufficient nonlinear accumulation, especially under the condition of CW pumping. Controlling the backward Rayleigh scattered light is the key to gain a high-power SC with unidirectional output in a single-stage RFL. Taking above into account, the introduction of a feedback device is applicable to obtain high-power SC with unidirectional output. Commonly, the feedback device is placed between the pump laser and the passive fiber to feed the backward Rayleigh scattered light to the forward direction. The broadband feedback is provided by a broadband mirror or coupler or fiber end feedback, and a wavelength division multiplexer (WDM) is included to act as a bridge [12-15]. This means that the WDM needs to withstand the high pump injecting, which also increases the complexity of system simultaneously. Based on this scheme, the maximum SC output power in a single-stage RFL was maintained at about 40 W [12]. Further power scaling is limited by the high-power processing capacity of the WDM.

In this paper, we propose an innovative structure to obtain kilowatt-level SC output based on a single-stage RFL with a half-open cavity. The broadband feedback is introduced by adding a
broadband coupler before the pump laser, which is more conducive to scale the SC output power and enhance the SC conversion efficiency compared with the feedback introduced after the pump laser. The random distributed feedback and the nonlinear accumulation are provided by a piece of long passive fiber. By a contrast, SC output performances in the system without the feedback are demonstrated. The results indicate that when the feedback is introduced, both the SC output power and the conversion efficiency have been apparently improved. Under the maximum pump power of 1847 W, a 1300 W SC with spectral range of 887-1920 nm and conversion efficiency of 66 % is obtained.

II. Experimental setup

Figure 1 shows the experimental setup for kilowatt-level SC generation. It is formed in a single-stage RFL with a half-open cavity. Specifically, the pump source used for bidirectionally pumping the fiber oscillator consists of 27 laser diodes (LDs) with central wavelength of 940 nm. The fiber oscillator has a central wavelength of 1080 nm and acts as the pump laser for SC generation. Both the forward and backward (18+1)×1 pump/signal combiners are used to couple the pump into a piece of 25/400 μm ytterbium-doped fiber (YDF) with a low pump absorption coefficient of 0.56 dB/m at 915 nm and a fiber length of 35 m. A pair of fiber Bragg gratings (FBGs) are placed on either side of the LMA YDF to form a resonant cavity, where the reflectivity of the high-reflectivity fiber Bragg grating (HR-FBG) and the output coupler fiber Bragg grating (OC-FBG) are 99.9 % and 6.2 % with a 3 dB bandwidth of 4 nm and 1 nm, respectively. Two separate cladding light strippers (CLSs) could effectively remove the residual cladding light. A 10/125 μm coupler with power ratio of 50:50 and working wavelength of 1160 ± 40 nm is used for broadband feedback, which is connected to the system with the help of a 10/125 μm -25/400 μm mode field.
adapter (MFA). A piece of 25/400 μm germanium-doped fiber (GDF) with a fiber length of 340 m is used to provide random distributed feedback and nonlinear accumulation. A homemade endcap is cleaved at an angle of 8° to avoid end feedback. The whole system of fiber oscillator is fixed on a water-cooled plate, and the long GDF is coiled in a water-cooled bucket. The coupler and MFA are placed on an aluminum plate for heat dissipation, and their temperatures are monitored by a thermal infrared viewer.

Fig. 1. The experimental scheme for kilowatt-level SC generation in a single-stage RFL with a half-open cavity. MFA, mode field adapter; HR FBG, high-reflectivity fiber Bragg grating; F-PSC, forward pump/signal combiner; YDF, ytterbium-doped fiber; OC FBG, output coupler fiber Bragg grating; B-PSC, backward pump/signal combiner; LD, laser diode; CLS, cladding light stripper; GDF, germanium-doped fiber.

III. Results and discussion

3.1 Single-stage RFL with a full-open cavity

The output spectrum of SC was collected by two optical spectrum analyzers (Yokogawa, AQ6374 and AQ6375) with spectral bands of 350 – 1750 nm and 1200 – 2400 nm respectively. The measured spectra were spliced together by aligning the spectral intensity.
Firstly, the broadband coupler is removed and the idle fiber output end of the HR-FBG is cleaved at an angle of 8° to prevent end feedback. The output end of the HR-FBG is defined as the backward output direction. The output performances of the RFL with a full-open cavity are measured. The spectral evolutions of forward and backward output laser are recorded in Fig. 2. The zero-dispersion wavelength (ZDW) of 25/400 µm YDF and GDF are about 1.3 µm. When the pump is located in the normal dispersion region of the fiber, the Raman effect dominates the initial spectrum expansion [16]. The spectrum of Fig. 2(a) appears three Raman peaks at maximum pump power which lies around 1134 nm, 1193 nm, and 1259 nm, and they all correspond to 13.2 THz downshift of previous signal wavelength. The higher-order Raman peak has the larger spectral bandwidth, benefiting from the broadband Raman gain spectrum of Raman effect[17]. For backward output spectrum in Fig. 2(b), the intensity of the 1134 nm first-order Raman peak is about 28 dB higher than that of the pump peak, which indicates that the backward output laser is basically concentrated in the first-order Raman peak.

The forward and backward laser output power are measured to quantitatively observe the laser output performance. Figure 3(a) plots the laser output powers versus the pump laser power in forward and backward directions, and corresponding conversion efficiencies are shown in Fig. 3(b). At first, the forward laser output power increases almost linearly with the injecting of pump laser. When the pump laser power reaches 575 W, the forward laser output power reaches the threshold for backward Rayleigh scattering, and the backward laser starts to appear. The backward laser obtains the active gain when it pass through the YDF, which is due to that the wavelength of backward laser (1134 nm) is located in the ytterbium ion radiation range of 1000-1200 nm. With the pump laser power increasing to 1185 W, the backward output power is amplified to 298 W with the aid of the distributed Raman gain and the active gain. In this process of power scaling,
the conversion efficiency of the forward laser has been decreasing. The forward first-order Raman laser and the pump laser have opposite intensity distribution along the GDF, resulting in the saturation of forward first-order Raman gain. The Raman gain saturation becomes increasingly obvious with the increase of the pump laser power [19]. As the pump laser power reaching the maximum value, the conversion efficiency of forward laser descends to 59% and the forward output power almost stops growing. It is caused by the combination effect of the Raman gain saturation of forward laser and the quantum defect occurring in the process of wavelength conversion in the forward direction. In [19], the backward first-order Raman output power always is higher than the forward first-order Raman output power due to the Raman gain saturation of forward laser. However, in our full-opened RFL at maximum pump laser power, the calculated forward and backward first-order Raman output power by the method of spectral integration are 443 W and 294 W, respectively. The lower backward first-order Raman output power is due to insufficient distributed backward scattering and the existence of the walk-off effect [11]. If further increasing the pump laser power, the energy pump may be completely transferred to the backward output laser due to the enhanced backward scattering, the Raman gain saturation of forward laser, and the quantum defect in the forward direction.
Fig. 2. Output spectral evolution of pump laser power in the RFL with a full-open cavity. (a) forward direction and (b) backward direction.

![Graph showing output spectral evolution](image)

Fig. 3. (a) laser output power and (b) conversion efficiency of the RFL with a full-open cavity in the both directions. The green background area is the growth area of the backward output power; the yellow background area shows that the forward output power stops increasing.

### 3.2 Single-stage RFL with a half-open cavity

![Comparison of output spectra](image)

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<tr>
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<th>Pump power</th>
<th>Forward output power</th>
<th>Backward output power</th>
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<tr>
<td>full-open cavity</td>
<td>964 W</td>
<td>653 W</td>
<td>286 W</td>
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<tr>
<td>half-open cavity</td>
<td>964 W</td>
<td>797 W</td>
<td>0.2 W</td>
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Fig. 4. The compared output spectra of RFLs with a full-open cavity and a half-open cavity under the same pump power of 964 W.
It could be discovered from the discussion above that the backward output power is rather high in the single-stage RFL with a full-open cavity. To solve this problem, a broadband coupler is supplied before pump laser to form a half-opened RFL. It is noted that in the RFL with a full-open cavity, the strong backward laser is obtained by the weak backward Rayleigh scattering light combined with the distributed Raman gain and ytterbium ion active gain. When the coupler is added, the gain competition occurs between the forward feedback light and the weak backward Rayleigh scattered light in the transmission process along the fiber. Part of energy is transferred to the forward laser and backward output power is reduced, which means that the coupler does not need to withstand too much power. It is roughly estimated by monitoring the coupler temperature and result shows that the temperature of the coupler has no obvious rise in the whole process of power scaling. Figure 4 shows the compared output spectra of RFLs with a full-open cavity and a half-open cavity under the same pump power of 964 W. The inset displays the forward and backward output power in both structures. The results demonstrate that, the backward output light is fed back into the forward direction with the aid of the broadband coupler, promoting forward output power and conversion efficiency. The output spectrum of the half-opened RFL is greatly expanded compared to that of the full-opened RFL under the same pump power. This is because the boosting of forward output power facilitates the interaction among nonlinear effects such as Raman effect, phase-matched four-wave mixing, and group-velocity matched dispersive wave, thus promoting the conversion among wavelengths.

As followed, the output performances of the RFL with a half-open cavity are analyzed in detail. Figure 5 presents its output spectral evolution. The mechanism of initial spectrum expansion is similar to that of the full-opened RFL, which is dominant by the cascaded Raman effect. The modulation instability (MI) starts to work and gives birth to a train of ultra-short pulses when the
long wavelength edge of spectrum is extended beyond ZDW of the fiber [19]. In the short wavelength direction, the whole Raman substrate is connected under combined action of dispersive waves trapped by soliton and phase-matched four-wave mixing [20]. In the long wavelength direction, the extension of spectrum is induced by soliton self-frequency shift and soliton fission [21]. With the further raising the pump power, these effects are stimulated more effectively and together enhance the broadening of spectrum. Although the combination of the CW pump and the LMA fiber with a low nonlinear coefficient is difficult to excite various nonlinear effects, the spectrum is broadened in effect, which is benefiting from the high pump power and the long interaction length of various nonlinear effects increased by random distributed feedback [6]. When the pump power reaches 1847 W, a broadband spectrum covering 887-1920 nm is then obtained.

Figure 6 presents the laser output power and the conversion efficiency versus the pump laser power in half-opened RFL. When the pump power reaches 1847 W, the SC output power reaches 1300 W. The conversion efficiency decreases with the increase of pump power due to the quantum defect occurring in the whole process of wavelength conversion. Concerning that for the final SC, the laser conversion efficiency reaches 66%, which is the highest conversion efficiency in reported RFL output SC with the same spectral range. Such high conversion efficiency is benefited by the introduced position of feedback in our structure. The feedback is introduced between the pump laser and the passive fiber, thus the SC output power is difficult to increase and the SC output spectrum and conversion efficiency are also relatively poor (see supplementary material for details). In our structure, the feedback is introduced before the pump laser, the backward scattered light passes through the YDF and experiences the ytterbium ion gain in bandwidth range of 1000-1200 nm. Then, both the 1000-1200 nm wavelength range backward light and the 1080 nm signal light extract energy from the 940 nm pump light, promoting the conversion of pump light and
enhancing the conversion efficiency. The bandwidth of the coupler is 1120-1200 nm. The light in the wavelength range will pass through the YDF multiple times due to the presence of the coupler with broadband strong feedback, further enhancing this effect. In addition, the bandwidth of the coupler covers the strong radiation wavelengths of backward light (1134 nm backward first-order Raman and 1193 nm backward second-order Raman). The coupler is fabricated by fused taper technique. The light located in the bandwidth of the coupler obtains the strong feedback, and the light located outside the bandwidth of the coupler also obtains the relatively weak feedback. With the aid of the coupler, the backward light losses is reduced and the conversion efficiency is improved efficiency.

![Figure 5](https://doi.org/10.1017/hpl.2023.66)

Fig. 5. Output spectral evolution with pump laser power in the RFL with a half-open cavity.
Fig. 6. (a) laser output power and (b) conversion efficiency in the RFL with a half-open cavity.
Fig. 7. The normalized temporal signal of the RFL with a half-open cavity. (a) spectrum expansion below ZDW; (b) spectrum expansion near ZDW; (c) spectrum expansion above ZDW; (d) Maximum spectrum broadening. The recorded time window is set to 100 ms.

The temporal behaviors of the half-opened RFL are measured in the output end by an InGaAs photo-detector with a bandwidth of 1 GHz and an oscilloscope with a bandwidth of 1.5 GHz. The standard deviation (STD) values displayed are used to characterize the temporal dynamic. The results are shown in Fig. 7. The RFL has the advantage of suppressing self-pulsing effect [22]. In the self-pulsing dynamics, the photon lifetime in the cavity plays a major role. The longer the photon lifetime in the cavity $\tau_c$, the more stable time domain due to the suppression of self-pulsing.

It can be calculated by the following formula [23]:

$$\tau_c = \frac{2nL}{c(-\ln R_1R_2 + 2\alpha l)}$$

Where $L$ is the length of the resonator, $l$ is the length of the gain fiber, $n$ is the refractive index of fiber, $R_1$ and $R_2$ are the two-side reflectivities of the resonator, $\alpha$ is the scattering loss. The length of the gain fiber is relative to the pump light. It refers to the fact that when the length of gain fiber is long, the saturable absorption effect in the weakly pumped portion of the gain fiber triggers the strong self-pulsing effect initiated by the relaxation oscillations, corresponding to the reduction of intracavity photon lifetime in the formula [23]. However, the length of the resonator is relative to the signal light. Concerning the cavity of RFL, multiple scattering caused by random distributed feedback increases length of the resonator, thus enhancing the photon lifetime in the cavity and leading to a stable CW operation[24]. With the increase of pump power, Rayleigh scattered light based on random distributed feedback is strengthened. On the one hand, the part of backward Rayleigh scattered light at the 1080 nm is amplified in the oscillator, reducing the time domain fluctuation of the 1080 nm signal light, the corresponding time domain properties is transferred.
from the signal light to subsequent Raman lights. On the other hand, the random distributed feedback of Raman light enhance the intracavity photon lifetime. Based on the above two aspects, a stable Raman laser output is obtained. As shown in Figs. 7(a)-7(b), the STD values indicate that the output laser becomes more and more stable with the increasing pump power during the whole conversion process of the Raman peak. When the spectrum extends beyond ZDW of the fiber, the slight time domain fluctuation could be observed in Fig. 7(c), which tends to be caused by nonlinear effects involving the process of SC broadening, such as soliton fission. Due to the generated pulse originating from the soliton fission has the random duration and energy, the pulse train with periodic modulation is not observed in the time domain. With the further increase of pump power, the time domain becomes more stable again owing to the increasing intracavity photon lifetime caused by enhanced random distributed feedback, which is shown in Fig. 7(d). The results indicate that this scheme could produce a stable SC laser source, especially during high-power operation.

**IV. Conclusion**

In conclusion, a novel experimental scheme is used to realize the kilowatt-level SC output. In the absence of feedback, the combination of Rayleigh scattering, distributed Raman gain, and active gain results in a high-power backward laser output, which limits the power scaling of the forward laser. By introducing the feedback before the pump laser, the backward power loss can be reduced and the pump can be fully utilized, which improves the forward output power and conversion efficiency significantly. At the maximum pump power of 1847 W, a 1300 W SC with a spectrum covering 887-1920 nm and an optical conversion efficiency of 66% is obtained. The output temporal behaviors illustrate that the RFL cavity can stably work. Compared with the reported RFL output SC, the experimental structure is the simplest and the conversion efficiency is the
highest in the same spectral range. This simple scheme not only can be used to generate high-power SC laser with high efficiency and sound robustness, but also presents rich phenomena, providing important reference significance for other lasers (such as Raman fiber laser and point-reflector-free RFL) as well as scientific research.

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