

# Will subglacial rhyolite eruptions be explosive or intrusive? Some insights from analytical models

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**ABSTRACT.** Simple analytical models of subglacial eruptions are presented, which simulate evolving subglacial cavities and volcanic edifices during rhyolitic eruptions beneath temperate glaciers. They show that the relative sizes of cavity and edifice may strongly influence the eruption mechanisms. Intrusive eruptions will occur if the edifice fills the cavity, with rising magma quenched within the edifice and slow melting of ice. Explosive magma–water interaction may occur if a water- or steam-filled gap develops above the edifice. Meltwater is assumed to drain away continuously, but any gap above the edifice will be filled by meltwater or steam. Ductile roof closure will occur if the glacier weight exceeds the cavity pressure and is modelled here using Nye's law. The results show that the effusion rate is an important control on the eruption style, with explosive eruptions favoured by large effusion rates. The models are used to explain contrasting eruption mechanisms during various Quaternary subglacial rhyolite eruptions at Torfajökull, Iceland. Although the models are simplistic, they are first attempts to unravel the complex feedbacks between subglacial eruption mechanisms and glacier response that can lead to a variety of eruptive scenarios and associated hazards.

## INTRODUCTION

The initial phases of subglacial eruptions occur within cavities melted into the glacier base by magmatic heat (e.g. Höskuldsson and Sparks, 1997; Wilson and Head, 2002; Guðmundsson, 2003). The eruptive behaviour involves interaction between rising magma and meltwater, which may lead to the formation of pillow lavas, quench-hyaloclastite or phreatomagmatic tephra, depending upon the mechanism of magma–water interaction (e.g. Moore and others, 1995; Smellie and Hole, 1997; Tuffen and others, 2001).

Studies of subaqueous volcanism have shown that the mechanism of magma–water interaction depends upon the confining pressure (e.g. Moore and Schilling, 1973), magma–water ratio (Wohletz, 1983), magma volatile content (McBirney, 1963; Dixon and others, 1995; Wright and others, 2003) and the ability of magma and water to mix (e.g. Zimanowski and others, 1997). Similarly, the mechanisms of subglacial eruptions are controlled by the cavity conditions such as confining pressure and abundance of meltwater (Tuffen, 2001; Kelman and others, 2002; Wilson and Head, 2002; Höskuldsson and others, 2006). These conditions may change very rapidly, even in non-volcanic areas (e.g. Kavanaugh and Clarke, 2000) and are determined by patterns of melting, ice deformation and meltwater drainage (e.g. Hooke, 1984; Björnsson, 1988). Since the melting rate during subglacial eruptions is itself determined by the eruption mechanisms (e.g. Guðmundsson, 2003), the eruption mechanism will in turn influence cavity conditions, and the volcano–ice system is coupled (Tuffen and others, 2001). The models presented here constitute a first attempt to simulate the behaviour of this coupled system.

## EXISTING MODELS OF SUBGLACIAL ERUPTION MECHANISMS

Many useful insights have come from recent models of subglacial eruption mechanisms. Höskuldsson and Sparks

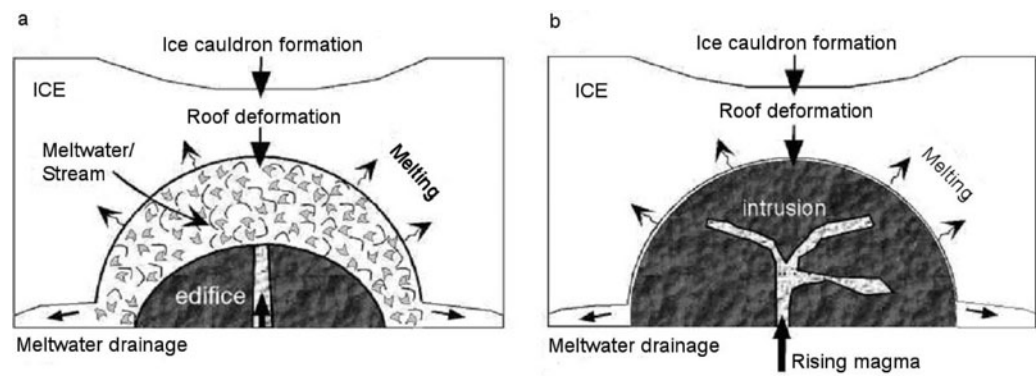
(1997) considered pressure changes during effusive eruptions within isolated cavities, from which meltwater cannot escape (closed system). Their calculations showed that the system volume will inevitably increase during effusion of rhyolitic magma, as the volume of ice melted is insufficient to accommodate the erupted magma. Volume increases were also predicted to occur during effusive basaltic eruptions, unless energy transfer was highly efficient (>80%) and the magma was vesicle-poor. The results were used to argue that meltwater may accumulate at the vent during some basaltic eruptions, but cannot do so during any rhyolitic eruption as an increase in volume will lead to increased pressure that will drive meltwater away from the vent area.

Tuffen and others (2002a) modelled localized melting of a glacier base during an intrusive rhyolite eruption. The competing effects of melting and inward ice deformation on the evolving size of the cavity were modelled using Nye's law (Nye, 1953). Tuffen and others (2002a) assumed that melting occurs evenly over the roof of a hemispherical cavity and that heat loss from magma was the rate-limiting step in the transfer of thermal energy from magma to ice, rather than the melting process itself. The validity of the latter assumption is brought into question by observations of the Gjálp eruption, as heated meltwater may have left the vent area (Guðmundsson and others, 2004).

Wilson and Head (2002) provided a novel approach to the mechanisms of subglacial basaltic eruptions, suggesting that dykes may propagate into the glacier base, melting narrow, blade-like cavities, and that the early stages of eruptions may be regarded as the intrusion of sills at the ice-bedrock interface. The dykes would collapse once the supporting ice was melted away.

## THE INFLUENCE OF CONFINING PRESSURE ON SUBGLACIAL ERUPTION MECHANISMS

Subglacial basaltic tuyas typically consist of basal pillow lavas overlain by increasingly vesicular hydroclastic tephra



**Fig. 1.** Representations of the (a) explosive and (b) intrusive styles of subglacial rhyolite eruptions modelled in this paper. There is a substantial gap above the edifice in (a), filled by meltwater or steam allowing explosive magma–water interaction to occur. In (b) the edifice completely fills the cavity and rising magma intrudes within the edifice. Modified from Tuffen (2001).

(e.g. Smellie, 2000), indicating that the mechanism of magma–water interaction changes during edifice growth as the confining pressure decreases. In general, pillow lavas generally form beneath ice  $\geq 500$  m thick and hydroclastic tephra beneath thinner ice (e.g. Moore and others, 1995), but there are exceptions to this rule, as other factors such as the magma volatile content, effusion rate and magma–water ratio are also important (e.g. McBirney, 1963; Wright and others, 2003; Griffiths and Fink, 1992; Wohletz, 1983). Explosive activity may also occur under thicker ice if subglacial pressures are less than glaciostatic (Wilson and Head, 2002; Schopka and others, 2006).

In contrast, there is no obvious relationship between stratigraphic position and facies type for the subglacial phase of rhyolite tuya-building eruptions. Eruptions appear to be either dominantly explosive, generating phreatomagmatic tephra, or intrusive, with the emplacement of quench hyaloclastite (Tuffen and others, 2001; Tuffen and others, 2002b; Stevenson, 2005). It thus appears that factors other

than confining pressure are of predominant importance during rhyolitic eruptions, most probably the effusion rate and magma volatile content.

CAVITY PRESSURE, MELTWER DRAINAGE AND ICE DEFORMATION

Höskuldsson and Sparks (1997) showed that cavity pressure in a closed system may be less than glaciostatic (with the difference here defined as the underpressure) if magma–ice energy transfer is highly efficient. Although such efficiency may seldom occur in real systems (Guðmundsson, 2003), underpressures may nonetheless develop if hydraulic connectivity with low-pressure cavities is established and meltwater drainage occurs (e.g. Wilson and Head, 2002; Schopka and others, 2006). Indeed, there is increasing evidence that meltwater can drain subglacially at the onset of most subglacial eruptions (e.g. Tuffen and others, 2001; Guðmundsson and others, 2004).

Cavity underpressures depend on aspects of the local hydrology such as tunnel length, meltwater flux and temperature (e.g. Hooke, 1984). Underpressure leads to inward roof deformation, which will be ductile if cavity radius  $\ll$  ice thickness. The deformation rate for cylindrical or spherical cavities is given by Nye’s law (Nye, 1953). Roof closure leads to depression of the ice surface above, forming an ice cauldron. As the cavity size increases, the ice eventually fails brittly, typically once the cauldron is  $\geq 50$  m deep (as observed in Iceland, e.g. Guðmundsson and others, 1997). The depth of brittle failure then increases as the cavity grows until the cavity roof fails and a subaerial eruption commences (Guðmundsson and others, 1997, 2004).

**Table 1.** Variables and constants used in the models. Data from Höskuldsson and Sparks, 1997

Symbol		Units
$Q$	Heat output	W
$E$	Energy/magma volume	$\text{J m}^{-3}$
$V$	Volume	$\text{m}^3$
$R$	Radius	m
$Q_i$	Effusion rate	$\text{m}^3 \text{s}^{-1}$
$r'$	Rate of change of radius	$\text{m s}^{-1}$
$v$	Ice melted/magma volume	–
$T$	Temperature	$^{\circ}\text{C}$
$\Delta T$	Temperature change	$^{\circ}\text{C}$
$P$	Pressure	Pa
$\Delta P$	Pressure difference	Pa
$\rho$	Density	$\text{kg m}^{-3}$
$c$	Specific heat capacity	$\text{J kg}^{-1} \text{ }^{\circ}\text{C}^{-1}$
$\theta$	Magma vesicularity	–
$t$	Time	s
$L$	Heat of fusion	$\text{J kg}^{-1}$
$g$	Gravitational constant	$9.81 \text{ m s}^{-2}$
$n$	Glen’s flow law constant	3
$B$	Ice viscosity law parameter	$5.3 \times 10^7 \text{ Pa s}^{1/3}$
$S$	Packing coefficient	–

Note: l–magma.

**Table 2.** Properties of ice and rhyolite magma (Höskuldsson and Sparks, 1997)

Symbol	Value and units
$T_i$	$0^{\circ}\text{C}$
$\rho_i$	$917 \text{ kg m}^{-3}$
$L_i$	$3.35 \times 10^5 \text{ J kg}^{-1}$
$T_l$	$900^{\circ}\text{C}$
$\rho_l$	$2300 \text{ kg m}^{-3}$
$c_l$	$1.04 \text{ kJ kg}^{-1} \text{ }^{\circ}\text{C}^{-1}$

Note: i–ice, l–magma.

## EVIDENCE FROM THE 1996 GJÁLP ERUPTION AND MODELS OF GUÐMUNDSSON

Observations and models of the 1996 Gjálp eruption, as described in Guðmundsson (2003) and Guðmundsson and others (1997, 2002, 2004) have provided important new constraints on many aspects of magma–ice interaction. The following information is useful for the models presented here: (1) Deformation of the 450–650 m thick ice above the eruption site was initially ductile. (2) Although meltwater drained from the eruption site, a column of meltwater accumulated above the edifice. (3) The well-drained subglacial cavity above the southern part of the fissure had an underpressure of about 2 MPa. (4) The heat transfer efficiency between magma and ice at the eruption site  $f_i$  was between 0.55 and 0.66. (5) Less than 10% of the erupted products were washed away by meltwater. (6) The heat flux during the eruption was 100 times that during slow cooling of the Gjálp edifice.

## OUTLINE OF THE MODEL

This paper employs a simple model of the volcano–ice system to explore the effects of various parameters on eruption mechanisms. It considers rhyolitic eruptions as point sources at the base of horizontal ice sheets with constant effusion rates. It is assumed that the feeder dyke does not overshoot the bedrock–ice interface (cf. Wilson and Head, 2002). Magmatic heating causes melting of ice, forming a hemispherical cavity at the glacier base (Fig. 1). The cavity roof closes by ductile deformation, approximated by Nye's law, at a rate determined by the cavity size and underpressure. The cavity size is determined by the relative rates of enlargement by melting and closure by ice deformation. Meanwhile, a volcanic edifice accumulates within the cavity (Fig. 1). Although meltwater is assumed to escape from the cavity, any gap above the edifice will be filled with water and steam (Fig. 1a). The model predicts the evolving sizes of the cavity and the edifice together with the depth of water/steam above the edifice and the depth of the ice cauldron (Fig. 2). A range of ice thicknesses, effusion rates and magma vesicularities is employed. Tables 1 and 2 list the variables and constants used.

### Heat transfer from magma to ice

The thermal energy released per unit volume of rhyolitic magma during cooling and quenching  $E$  is given by

$$E = (1 - \theta)\rho_l c_l \Delta T_l \quad (1)$$

where  $\theta$  denotes magma vesicularity,  $\rho_l$  the unvesiculated magma density,  $c_l$  magma heat capacity and  $\Delta T_l$  the temperature change of the magma (Höskuldsson and Sparks, 1997). This assumes that (1) the deposits are glassy, which is appropriate for the vast majority of subglacial rhyolites studied, so that the latent heat of crystallisation can be ignored, and (2) the heat capacity of gases within vesicles is negligible.

### Mechanisms and efficiency of heat transfer

Only heat released rapidly from the magma is considered (within seconds or minutes of its emplacement); later edifice cooling is ignored. The heat transfer efficiency  $f_i$  is the fraction of heat transferred instantaneously to melt the ice

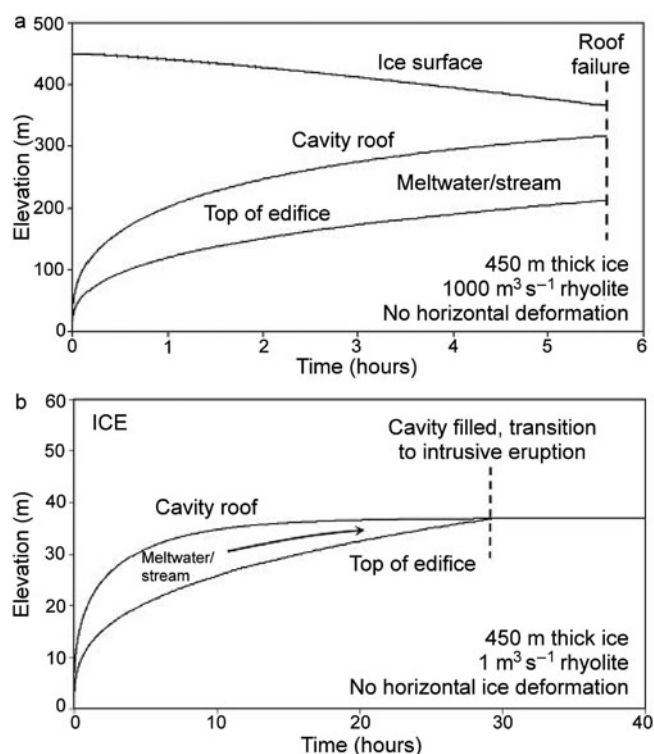


Fig. 2. Model results for (a) large and (b) small effusion rate eruptions beneath ice 450 m thick, indicating the changing elevation of the edifice radius, cavity radius and, in (a) only, the ice surface.

(Guðmundsson and others, 2004). Therefore, the heat flux for ice melting,  $Q_m$ , is equal to

$$Q_m = Q_{l(t)} E f_i \quad (2)$$

where  $Q_{l(t)}$  is the instantaneous effusion rate and  $E$  is the total thermal energy of the magma as before. The heat transfer efficiencies for two possible eruption mechanisms are considered. During (a) phreatomagmatic fragmentation, heat loss from magma is rapid due to the large surface area for heat exchange (Zimanowski and others, 1997). Heat loss models and observations from Gjálp suggest that  $f_i$  may range between 0.55 and 0.66 (Guðmundsson, 2003), but for simplicity and because these models are only approximate, a value of 1 will be used for these models. During (b) intrusive eruptions, rising magma is quenched by meltwater within the slowly cooling edifice (Tuffen and others, 2002a). The heat transfer rate is much smaller than during phreatomagmatic fragmentation and is similar to that from a newly erupted edifice. As the heat flux from the Gjálp edifice immediately after the eruption was approximately 5–10% of the heat flux during it (Guðmundsson and others, 2004),  $f_i$  is estimated to be 0.1.

### Melting of ice

Magmatic heat may cause melting of ice and also heating and vaporization of the meltwater. Although meltwater temperatures may be 20°C or more (Guðmundsson and others, 1997), for simplicity meltwater will be assumed to be at 0°C. The fraction of heat converted to kinetic energy during phreatomagmatic explosions is likely to be small (Wohletz, 1983) and will be ignored. The volume of ice



melted per unit volume of magma  $v_i$  is thus given by

$$v_i = \frac{f_i}{\rho_i L_i} [c_i \rho_i \Delta T_i (1 - \theta)] \quad (3)$$

where  $\rho_i$  and  $L_i$  are the density and heat of fusion of ice, respectively.

It is assumed that melting occurs evenly over the roof of a hemispherical cavity of radius  $R$ . The melt-back rate  $r'_m$  is thus given by

$$r'_m = \frac{v_i Q_1}{2\pi R^2} \quad (4)$$

where  $v_i$  is the volume of ice melted per unit volume of magma and  $Q_1$  is the effusion rate.

### Ice deformation

According to Nye's law, the roof of a hemispherical cavity within an infinite ice sheet will deform at a rate  $r'_d$  given by

$$r'_d = R \left( \frac{\Delta P}{nB} \right)^n \quad (5)$$

where  $\Delta P$  is the cavity underpressure,  $n$  is Glen's flow law constant ( $\approx 3$ ) and  $B$  is an ice deformation parameter, taken as  $5.3 \times 10^7 \text{ Pa s}^{1/3}$  (e.g. Hooke, 1984).

Nye's law applies when the cavity radius is small compared with the ice thickness (Nye, 1953) but breaks down at large cavity sizes. The simulations have been run until the ice roof is less than 50 m thick, when it is assumed to fail. The results will therefore only be approximate at large cavity sizes, once Nye's law begins to break down.

Ice will flow horizontally into the ice cauldron, as its surface seeks to regain an equilibrium shape (Aðalgeirsdóttir and others, 2000). At Gjalp, deformation speeds were approximately  $10^{-5}$ – $10^{-6} \text{ m s}^{-1}$ , meaning that substantial changes in the surface profile would require years. To illustrate this, at a reasonable range of effusion rates of  $1$ – $100 \text{ m}^3 \text{ s}^{-1}$  for silicic dome-building eruptions and  $10^3$ – $10^6 \text{ m}^3 \text{ s}^{-1}$  for plinian eruptions (Pyle, 2000), we find that a 500 m high hemispherical edifice would be constructed in months to years during a dome-type eruption and hours to days in plinian eruptions. This suggests that horizontal closure beneath ice thicknesses of the order of 500 m may only be significant during prolonged eruptions with small effusion rates. Nonetheless, two end member scenarios are envisaged in the models: one in which no horizontal ice deformation occurs, the other where closure is so rapid that the surface remains horizontal at all times (here termed 'perfect horizontal deformation').

### Cavity pressure and roof closure

For the purposes of this study, cavities are assumed to be at atmospheric pressure due to meltwater drainage and the establishment of a hydraulic connection with low-pressure cavities. Although this may be unrealistic for some eruptions, it avoids the difficulty of estimating cavity pressures, which depend on so many aspects of the local hydrology and the melting process. A justification for this assumption is that many rhyolitic eruptions occur at central volcanoes with powerful geothermal systems (e.g. Torfajökull, Krafla and Kerlingarfjöll). There is therefore likely to be a high geothermal heat flux in the vicinity of the vent directly preceding the eruption, which would favour the development of low-pressure cavities, as found in the firn-filled crater of Mount Rainier where there is a strong

geothermal field (Kiver and Steele, 1975). The rates of ice deformation predicted by the model are therefore maximum rates. Models exploring the effects of different cavity pressures on the mechanisms of subglacial eruptions will be presented elsewhere.

The glaciostatic pressure at the cavity roof  $P_{g(t)}$  at time  $t$  is given by

$$P_{g(t)} = \rho_i g h_{r(t)} \quad (6)$$

where  $h_{r(t)}$  is the ice roof thickness at time  $t$ , expressed as

$$h_{r(t)} = h_0 - R_{(t)} - \int_0^t r'_{d(t)} dt = h_0 - \int_0^t r'_{m(t)} dt \quad (7)$$

where  $h_0$  is the initial ice thickness and  $r'_m$  is the melt-back rate as defined in Equation (4). The pressure driving deformation of the cavity roof,  $\Delta P_{(t)}$  is given by

$$\Delta P_{(t)} = \rho_i g h_{r(t)} - P_c = \rho_i g \left[ h_0 - \int_0^t r'_{m(t)} dt \right] - P_c \quad (8)$$

where  $P_c$  is the cavity pressure, assumed to be 0.1 MPa in these simulations. Note that when there is no horizontal deformation, the roof will progressively thin during the eruption, reducing the weight of the ice roof and leading to slower rates of closure.

### Cavity size balance

The cavity size is determined by the relative rates of enlargement by melting and closure by deformation. The rate of cavity enlargement  $dR/dt$  is thus given by the relation:

$$\frac{dR}{dt} = r'_m - r'_d \quad (9)$$

Substituting Equations (4) and (5) into Equation (9) yields

$$\frac{dR}{dt} = \frac{v_i Q_1}{2\pi R^2} - R \left( \frac{\Delta P}{nB} \right)^n \quad (10)$$

where  $Q_1$  is the volume flux of magma ( $\text{m}^3 \text{ s}^{-1}$ ). Equations (3) and (8) can therefore be combined with Equation (10) to give

$$\frac{dR}{dt} = \frac{Q_1}{2\pi R^2} \left[ \frac{c_i \rho_i \Delta T_i (1 - \theta)}{\rho_i L_i} \right] - R \left[ \frac{\rho_i g \left[ h_0 - \int_0^t r'_{m(t)} dt \right] - P_c}{nB} \right]^n \quad (11)$$

which provides the changing cavity size with time. Solutions to Equation (11) are approximated numerically using a spreadsheet program. Values of melt-back rate, ice deformation rate and cavity radius are calculated incrementally for a series of time steps such that  $t_{n+1} = 1.01 t_n$ . Simulations are continued until the roof is less than 50 m thick, which typically takes  $10^6$ – $10^7$  s. Roof failure will then lead to a subaerial eruption. The cavity radius initially increases rapidly ( $dR/dt \sim 10^{-2}$ – $10^{-3} \text{ m s}^{-1}$ ), because the melting occurs over a small area and roof closure is slow. As the cavity size increases, the melt-back rate reduces and roof closure accelerates, although substantial roof thinning will reduce the closure rate.

### Edifice volume and space in cavity

The edifice volume  $V_e$  is given by

$$V_{e(t)} = \int_0^t Q_1 S dt \quad (12)$$

where  $S$  is a packing coefficient, taken to be 1 for intrusive lava and 2 for pyroclastic deposits. It is assumed that a

negligible amount of material is removed by meltwater, justified by the estimate that only 10% of the Gjálþ products were washed away (Guðmundsson and others, 2004). The edifice radius is thus given by

$$R_{e(t)} = \left[ \frac{3V_{e(t)}}{2\pi} \right]^{1/3} = \left[ \frac{3 \int_0^t Q_1 S dt}{2\pi} \right]^{1/3} \quad (13)$$

Two scenarios are envisaged, one in which the edifice is considerably smaller than the cavity (A), and one in which the cavity is completely filled by the edifice (B).

#### A. Edifice radius < cavity radius

There will be a significant water column above the growing edifice, meaning that rising magma can interact with abundant meltwater. This allows potentially explosive magma–water interaction to occur (Figs 1a and 2a). The development of convection cells in the water may assist transfer of heat from fragmenting magma to ice, leading to rapid melting.

#### B. Edifice fills cavity

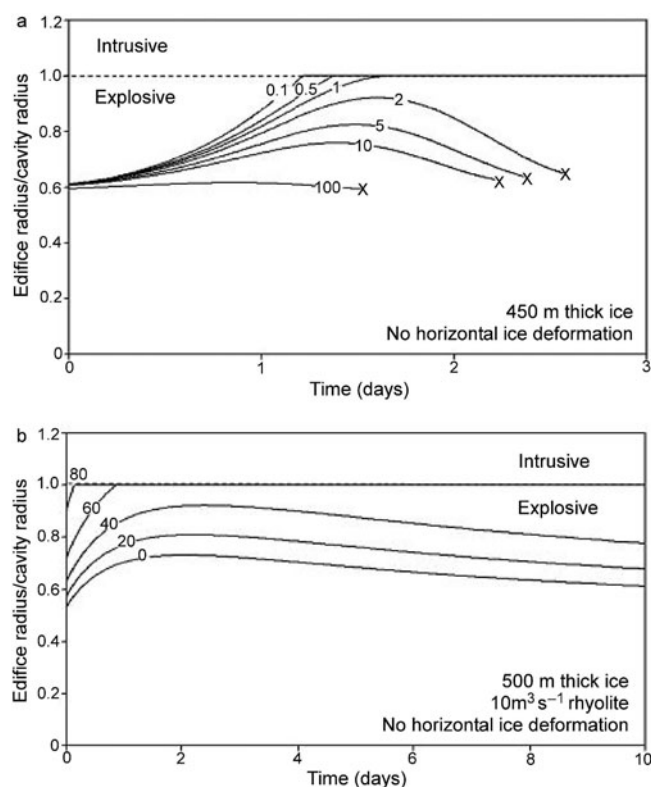
If the edifice fills the cavity, rising magma cannot interact with a column of water (Figs 1b and 2b). Instead, it is likely to intrude and be quenched within the poorly consolidated, waterlogged edifice. This may generate facies similar to pumiceous peperites (Hunns and McPhie, 1999; Tuffen and others, 2001), where the explosivity of the magma–water interaction is suppressed by the surrounding fragmental material, despite the magma being volatile-rich. A small proportion of the magma may reach the glacier base, where it may generate small ice caves through localized melting (Tuffen and others, 2002a) or intrude as a sill at the bedrock–ice interface (Wilson and Head, 2002).

### RESULTS OF THE MODELS

The model calculates the radii of the growing edifice and evolving subglacial cavity, together with the ice surface elevation. Figure 2 shows typical graphs produced using the model, for two values of effusion rate beneath ice 450 m thick. Deformation is insignificant when the effusion rate is large. Melting is more rapid (Fig. 2a) than roof closure and a considerable water- or steam-filled gap develops above the edifice until roof failure, when the cauldron is ~70 m deep. The smaller effusion rate leads to slower melting, and ice deformation becomes more important (Fig. 2b). With time, the edifice begins to fill the cavity (see arrow on Fig. 2b), leading to an intrusive style of eruption. Once cavities become filled, it is assumed that eruptions will remain intrusive as the heat flux to the glacier is greatly reduced. The evolving ratio of edifice radius to cavity radius for a range of effusion rates is displayed in Figure 3a, illustrating how cavities become filled at small effusion rates but a considerable meltwater/steam-filled gap develops at large effusion rates. The effects of magma vesicularity are shown in Figure 3b. If all other parameters are unchanged, increasing the magma vesicularity can lead to the cavity becoming filled at intermediate effusion rates. This is due to the smaller amount of heat per unit volume carried by highly vesicular magma.

#### Will eruptions be explosive or intrusive?

Solutions were found for the critical effusion rate  $Q_{cr}$  for a given ice thickness and with either no or perfect horizontal

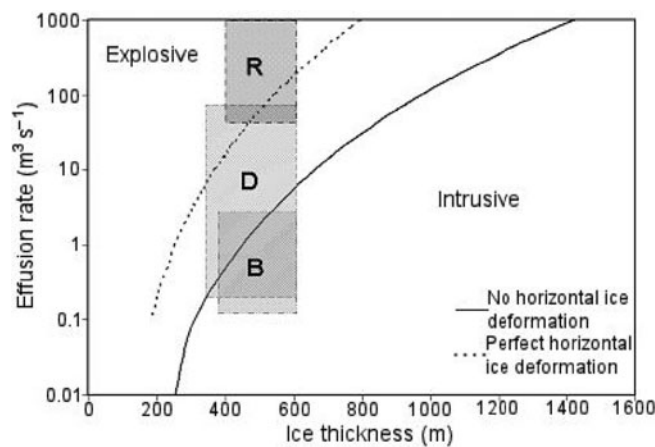


**Fig. 3.** Ratio of edifice radius to cavity radius during eruptions. Once the ratio becomes equal to 1, the eruption becomes intrusive and is assumed to remain so. (a) Results for eruptions with a range of effusion rates ( $Q_1$  values indicated) beneath ice 450 m thick. X indicates when the roof is <50 m thick and fails, so that eruptions become subaerial. (b) Results for variably vesicular magma under ice 500 m thick (% vesicularity indicated). When the vesicularity is small, there is sufficient melting to maintain space above the edifice and explosive eruptions occur. Greater vesicularities lead to filling of the cavity and the transition to intrusive eruptions.

ice deformation. At rates less than  $Q_{cr}$ , the cavity becomes completely filled by the edifice, which is likely to lead to an intrusive eruption mechanism. Above  $Q_{cr}$ , the edifice never completely fills the cavity, and the eruption has the capacity to remain explosive until it becomes subaerial. This process was repeated for a range of ice thicknesses, and the results plotted on Figure 4. Intrusive eruptions are favoured by thick ice and small values of  $Q_1$ . In addition to the main part of the modelling, it has also been shown that high meltwater temperatures and low cavity pressures favour intrusive eruptions (Tuffen, 2001), although these parameters are themselves dependent on the melting rate and eruption mechanisms and so are not strictly independent.

#### Models applied to subglacial rhyolite at Torfajökull, Iceland

Quaternary rhyolite eruptions at Torfajökull, Iceland occurred beneath ice >350 m in thickness and formed edifices between <0.1 and  $1 \text{ km}^3$  in volume (Tuffen, 2001). The lithofacies formed indicate that eruptions are either predominantly intrusive or explosive, although at one locality both styles of eruption appear to have occurred (Tuffen and others, in press). The effusion rate required to give each style of eruption was calculated for a plausible range of ice thicknesses and is shown in Figure 4.



**Fig. 4.** The critical effusion rate  $Q_{cr}$  plotted as a function of ice thickness. The two curves represent the two end-member scenarios: no and perfect horizontal ice deformation. The shaded fields illustrate plausible effusion rates and ice thicknesses for subglacial rhyolite eruptions at Torfajökull: B-Bláhnúkur, D-Dalakvísl, R-SE Rauðufossafjöll. Modified from Tuffen (2001).

### Intrusive eruption: Bláhnúkur

Less than  $0.1 \text{ km}^3$  of rhyolitic magma was erupted beneath  $>350 \text{ m}$  of ice at Bláhnúkur, with meltwater draining away from the vent area. The eruption was characterized by an intrusion of lava bodies into water-saturated hyaloclastite (Furnes and others, 1980; Tuffen and others, 2001) and the glacier base was close to the growing edifice throughout the eruption (Tuffen and others, 2002a). The eruption at Bláhnúkur therefore corresponds to the 'intrusive eruption' scenario described in the models and required  $Q_1 < \sim 10 \text{ m}^3 \text{ s}^{-1}$  for a plausible range of ice thicknesses (400–600 m), assuming that horizontal ice deformation was insignificant (Fig. 4). The edifice volume therefore implies an eruption duration of  $>4$  months.

An independent estimate of the effusion rate at Bláhnúkur is provided by Höskuldsson and Sparks (1997), based on buoyant rise of rhyolitic magma in a dyke. Their estimate of  $1\text{--}10 \text{ m}^3 \text{ s}^{-1}$  is consistent with our model results.

### Explosive eruption: Southeast Rauðufossafjöll

At Southeast Rauðufossafjöll, at least  $1 \text{ km}^3$  of magma was erupted beneath  $>400 \text{ m}$  of ice, forming a flat-topped tuya (Tuffen and others, 2002b). Massive fine-grained tephra  $>300 \text{ m}$  thick was emplaced during the subglacial phase during explosive magma–water interaction in a well-drained water- or steam-filled cavity. This eruption corresponds to the 'explosive eruption' scenario. According to the model, the effusion rate must have exceeded  $100 \text{ m}^3 \text{ s}^{-1}$  for a plausible range of ice thicknesses (Fig. 4). Using the magnitude-intensity relationships for recent and historical eruptions given in Pyle (2000), the effusion rate expected for a plinian eruption of this volume ( $1 \text{ km}^3$ ) is approximately  $10^4\text{--}10^5 \text{ m}^3 \text{ s}^{-1}$ . This would clearly be sufficient to sustain an explosive eruption, according to the models.

### Mixed explosive-intrusive eruption: Dalakvísl

A subglacial eruption at Dalakvísl, Rauðufossafjöll, was intermediate in style, including both explosive and intrusive phases (Tuffen and others, in press) (Fig. 5). The explosive phase initially involved fragmentation of  $>70\%$  vesicular

magma within a subglacial cavity, but this gave way to foam collapse and the rising magma began to be trapped and quenched within the vesicular deposits. The relatively high dissolved water content ( $>0.5 \text{ wt}\%$ ) measured using Fourier Transform Infrared (FTIR) spectroscopy on samples of the intruded lava indicates that this transition was not due to the exhaustion of magmatic volatiles (Tuffen and others, in press). Instead, it appears that the poorly-consolidated tephra had filled the cavity and was intruded by partly-fragmented foam, which no longer had the space to fragment or opportunity to interact explosively with meltwater. The highly vesicular nature of the magma may have encouraged the cavity to fill, due to the small amount of thermal energy carried per unit volume of the magma (Fig. 3b).

## DISCUSSION

Our model suggests that the effusion rate and ice thickness are important parameters influencing the mechanisms of subglacial rhyolite eruptions. The effusion rates required for intrusive and explosive eruptions at Torfajökull are consistent with independent estimates. Viewed broadly, the explosive eruptions are equivalent to plinian eruptions and the intrusive eruptions to effusive eruptions, although the elevated volatile contents in intrusive facies (Tuffen and others, in press) suggest that these contrasting styles are principally due to contrasting cavity conditions rather than different degrees of degassing. This contrasts with basaltic eruptions, where cavity pressures appear to be more important (e.g. Guðmundsson and others, 2004).

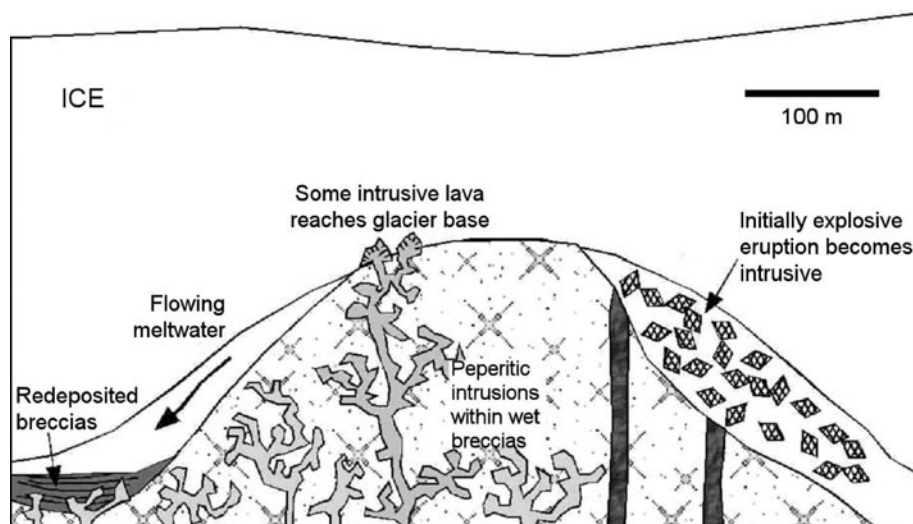
An explanation may be related to the initial volatile content of the magma. Whereas modest ( $\sim 5 \text{ MPa}$ ) changes in cavity pressure may significantly affect the vesiculation and ascent of water-poor basaltic magma (Höskuldsson and others, 2006), rhyolitic magma may be so water-saturated that the bulk of vesiculation occurs beneath the glacier base, reducing the impact of such pressure changes on its rate of ascent. This highlights the need to understand the relationship between volatile degassing, effusion rate and subglacial eruption mechanisms more fully, and this will be investigated in future work.

Alternatively, the lack of palagonitisation in subglacial rhyolitic deposits may explain the difference, meaning that they remain loose and waterlogged even during sustained eruptions. This makes it more difficult for rising magma to reach the glacier base: instead it is trapped and quenched within the edifice. In contrast, basaltic hyaloclastite rapidly palagonitises (Jakobsson, 1978), possibly fast enough to cause cementation during eruptions and facilitate propagation of dykes through to the glacier base.

Regarding glacier hydrology and cavity pressures, it is important to remember that the models developed here are simplistic, and represent only a first step towards the formulation of a general model of subglacial rhyolite eruptions. In addition to magma volatile contents, other issues to further consider include cavity morphologies (Höskuldsson and Sparks, 1997; Wilson and Head, 2002) and how cavity pressures are influenced by the glacier and bedrock topography, melting rate and the existing subglacial cavity system (e.g. Björnsson, 1988; Guðmundsson and others, 2004; Höskuldsson and others, 2006).

Finally, our models predict that ice cauldron depths may depend on the effusion rate, with the deepest cauldrons formed in small effusion rate eruptions when there is most





**Fig. 5.** An illustration of the mechanisms of the subglacial rhyolite eruption at Dalakvísl, Torfajökull (after Tuffen and others, 2007). In one location, an initially explosive eruption within a subglacial cavity became intrusive, apparently when the cavity was filled with tephra. Elsewhere, intrusive lava lobes were emplaced within waterlogged hyaloclastite breccias, some quenching at the glacier base. This may reflect changes in the effusion rate during the eruption. Meltwater drained away subglacially during the eruption.

time for ice surface deformation. Although these models only poorly simulate the formation of ice cauldrons, as brittle processes are clearly important, they do raise the intriguing possibility that apparent palaeo-ice thicknesses, as recorded by the ash-lava transition at tuyas, may depend upon the effusion rate, making palaeoclimatic reconstructions more difficult. This highlights the need for more attempts to quantitatively model ice deformation and melting during subglacial eruptions, and to improve our understanding of past climate as well as the hazards from explosive eruptions and jökulhlaups.

## CONCLUSIONS

The results of simple models of subglacial rhyolite eruptions suggest that their mechanisms are influenced by the effusion rate and ice thickness. At small effusion rates, subglacial cavities may become completely filled with volcanic debris as roof closure is important, favouring an intrusive style of eruption. At larger eruption rates, there is always space in the cavity for an explosive eruption to occur, due to the faster rate of melting. The models are used to estimate the effusion rate during some Quaternary eruptions at Torfajökull and the values found are consistent with independent estimates. This has been a first attempt to model the feedbacks between eruption mechanisms, ice melting and ice deformation during subglacial eruptions, and illustrates the challenge the complexly coupled volcano–ice system poses for future modellers.

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