THERMAL CONDUCTIVITY OF ICE IN THE TEMPERATURE RANGE 0.5 TO 5.0 K

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ABSTRACT. A method is described for measuring the thermal conductivity of ice in the temperature range from 0.5 to 5.0 K using a 3He apparatus. The results from our first experiments are not too far from the theoretical law for the low-temperature thermal conductivity of ice $\lambda = 0.42T^3$. Measurements at still lower temperatures are necessary to confirm our results.

INTRODUCTION

Callaway (1959) showed that the thermal conductivity coefficient $\lambda$ of a dielectric crystal can be expressed as:

$$\lambda = \frac{kT^3}{2\pi^2\hbar} \left(\frac{k}{\hbar}\right)^3 \int_0^{\Theta/T} r\tau^4 c^2 (c^2 - 1)^{-2} dx + \lambda_2,$$

(1)

where $\tau = \hbar\omega/kT$, $k$ is Boltzmann's constant, $T$ is the absolute temperature, $2\pi\hbar$ is Planck's constant, $\omega$ is the phonon frequency, and $\Theta$ is the Debye temperature. The total relaxation time $\tau$ is obtained by using the equation

$$\tau^{-1} = \sum_{i=1}^{n} \tau_i^{-1},$$

(2)

where the $\tau_i$ are the relaxation times corresponding to different phonon interaction mechanisms.

As Klinger (1975) pointed out, the correction term $\lambda_2$ can be neglected for ice samples, and the relaxation time due to phonon interaction with crystal imperfections can be written as:

$$\tau_d^{-1} = G_d\omega^R,$$

where $R$ takes the values 2 or 3 depending on the origin of the sample.

In order to describe phonon–phonon interactions it is sufficient to use a relaxation time for umklapp processes given by

$$\tau_u = 1.75 \times 10^{-17}\omega^2T \exp \left(-\Theta/6.5T\right).$$

(4)

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According to Casimir (1938) the thermal conductivity coefficient depends on a constant relaxation time
\[
\tau_e^{-1} = v/L_e, \tag{5}
\]
at sufficiently low temperatures at which the phonons are scattered at the boundaries of the sample. Here \( L_e \) is the Casimir length given by:
\[
L_e = 2H(ab/\pi)^{1/2}, \tag{6}
\]
with \( a \) and \( b \) the sides of the crystal parallelepiped perpendicular to the heat flow. \( H \) is a coefficient near to one due to the finite length of the sample.

In this case the thermal conductivity coefficient can be approximated by:
\[
\lambda = \frac{kL_e}{2\pi^2\nu^2} \left( \frac{kT}{\hbar} \right)^3 \int_0^\infty x^4 e^x (e^x - 1)^{-2} \, dx. \tag{7}
\]

As the temperature region where Equation (7) is valid could not be attained in his experiments, Klinger (1975) used a Casimir length calculated from Equation (6) with \( H = 1 \) in order to fit his experimental results. This method is only valid if the chosen mean value of the sound velocity is the most appropriate one. On the other hand if there are small-angle grain boundaries present in the crystal, the "apparent Casimir length", will be smaller than that calculated from the macroscopic crystal. As an incorrect value for \( \tau_e \) can lead to erroneous
parameters in Equation (3), it is necessary to measure the heat conduction directly in the
temperature region where Equation (7) is valid in order to give a more reliable interpretation
of the influence of lattice defects on low-temperature heat conduction data for ice. This is the
purpose of the present work.

EXPERIMENTAL PROCEDURE

Heat conduction experiments have been done between 0.58 K and 4.01 K on a \(^3\)He-
apparatus at the Service des Basses Tempéatures, Centre d’Études Nucléaires de Grenoble.
The major difficulty was to ensure a good thermal contact between the sample and the
cooling bath. As ice is very fragile, it was not possible to ensure a sufficiently good contact by
pressing the sample between copper plates as Klinger (1975) did at higher temperatures.
As the thermal dilatation coefficient of ice is very much higher than that of copper it is not
possible to freeze the crystal on a compact copper block.

We developed the sample holder shown in Figure 1 which gave good results: a small
Plexiglas (polymethylmethacrylate) vessel contained a loose bundle of 340 tinned copper
wires each 0.15 mm in diameter. These wires were related to the \(^3\)He bath.
The sample mounting was done in a cold room at 257 K. We introduced supercooled
water into the vessel and froze the sample to the copper wires. The cooling down of the sample
from cold-room temperature to liquid-nitrogen temperature was done at a rate of about
0.6 K/min.

We applied the steady-state heat-flow method and computed the thermal conductivity
coefficient from Fourier’s law:

\[ \lambda = \frac{P l}{ab\Delta T}, \]

where \(P\) is the power applied to the sample, \(a\) and \(b\) the section of the sample, \(l\) is the distance
between thermometers, and \(\Delta T\) the measured temperature difference.

We used two Allen Bradley carbon resisters as thermometers. The carbon resistor at the
“hot” side of the sample was calibrated by comparing it to a “Cryo Resistor” germanium
resistance of known characteristics. On the basis of this calibration the absolute temperature
of the carbon resistor was computed using an empirical law. The heater delivering the power
\(P\) was a strain gauge of 110 \(\Omega\). Another heating device fixed on the sample holder allowed us
to elevate the temperature of the sample without applying power to it. In order to eliminate
errors due to radiation and conduction in the heating wires, we used the double heating
method.

We apply a known power to the sample and read the values of the two resistance thermo-
meters. Then we heat the sample holder without applying power to the sample until the
temperature of the thermometer near to the heat sink is at the same value. \(\Delta T\) is given by the
difference of the temperatures indicated by the calibrated carbon resistor near to the heat
source and the absolute temperature by the mean value indicated by the calibrated thermo-
meter in the two cases.

The dimensions of the sample used were:

\[ a = 0.561 \pm 0.003 \text{ cm}, \]
\[ b = 0.588 \pm 0.003 \text{ cm}. \]

The distance between thermometers was:

\[ l = 4.05 \pm 0.05 \text{ cm}. \]

This gives us a form factor:

\[ l/ab = 12.3 \pm 0.3 \text{ cm}. \]
EXPERIMENTAL ERRORS

The error on the form factor given by Equation (9) affects only the absolute value of \( \lambda \). The systematic error due to the variation of \( \lambda \) in the temperature interval \( \Delta T \) can be neglected if we take care to satisfy the condition \( \Delta T/T < 5\% \).

Accidental errors are essentially due to the measurement of \( \Delta T \). It is not possible to evaluate these errors in a general manner as errors in \( \Delta T \) depend simultaneously on the sensitivities of the carbon resistors and on the fact that the power dissipated in the resistors has to be negligible compared to the power applied to the sample. This fact limits the sensitivity of the detection device. In general we can say that these errors are situated between 6 and 20\%. In one exceptional case it was as large as 60\%. Error bars are given for all results in Figure 2.

RESULTS

Five runs of the thermal conductivity measurements have been done on one sample cut perpendicular to the \( \varepsilon \)-axis within the temperature range from 0.58 to 4.01 K. The results are

![Graph showing thermal conductivity measurements](https://www.cambridge.org/core).
indicated in Figure 2. Qualitatively the interactions of phonons with crystal imperfections seem to become ineffective at temperatures as low as 1.5 to 1.2 K. For still lower temperatures a law $\lambda \propto T^3$ seems to be verified.

The points of run 4 are slightly displaced to lower values compared to the points of runs 1, 2, 3, and 5.

The extrapolation of our values to higher temperatures using thermal conductivity values from Klinger (1975) obtained on crystals with comparable crystallographic orientation suggests the existence of a maximum of thermal conductivity between 2 and 9 K.

**Discussion**

The value of the integral in Equation (7) is $\frac{4\pi^4}{15}$. If we take $\mu = 1$ since the sample length is much greater than $a$ and $b$, Equation (6) gives us the Casimir length $L_c = 0.65$ cm, and if we use as mean value of the sound velocity $v = 2.5 \times 10^5$ cm/s, Equation (7) gives us a low-temperature law of thermal conductivity of the form

$$\lambda = 0.42 T^3. \quad (10)$$

This is not too far from our experimental results as shown in Figure 2 if we take into account that we took a mean value of the sound velocity for the computation of the factor in Equation (10).

We were not able to explain in a satisfying manner the slight systematic displacement of run 4 relative to the other runs. A loss of power due to incomplete pumping of the exchange gas seems to be excluded as it would result in higher apparent $\lambda$ values. Further the apparent $\lambda$ values would depend on the applied power. In run 3 we repeated the measurements with different applied powers, but there was no important change in $\lambda$. It seems more plausible to explain the systematic deviation by a slight overheating of the calibrated carbon resistor due to a higher measuring current suggesting in this way a higher apparent $\Delta T$.

A definite answer whether or not we attained the region of constant mean free path can only be given if we are able to extend our measurements to still lower temperatures. Those measurements will give us at the same time information concerning which conditions of sample preparation lead to specular reflection of the phonons at the boundaries of the sample. A definitive interpretation of the type of interaction of phonons with defects in ice would seem possible when we have extended the range of heat conduction measurements on one sample from say 0.1 K to 20 K (the temperature where the influence of phonon scattering on defects becomes negligible compared to phonon-phonon interactions of the "umklapp" type (see Klinger, 1975)). This work is in progress in our laboratory.

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**References**

